

**GATE 2021**

**Electronics and Communication Engineering (EC)**

**General Aptitude (GA)**

**Q.1to Q.5 Multiple Choice Question (MCQ), carry ONE mark each (for each wrong answer : – 1/3).**

Q.1 The current population of a city is 11,02,500. If it has been increasing at the rate of 5% per annum, what was its population 2 years ago?

- (a) 9,92,500
- (b) 9,95,006
- (c) 10,00,000
- (d) 12,51,506

Ans. c

Exp:

$$1102500 = x \left( 1 + \frac{5}{100} \right)^2$$

$$x = 10,00,000$$

2. p and q are positive integers and

$$\frac{p}{q} + \frac{q}{p} = 3,$$

Then,  $\frac{p^2}{q^2} + \frac{q^2}{p^2} =$

- (a) 3
- (b) 7
- (c) 9
- (d) 11

Ans. b

Exp:

Given,  $\frac{p}{q} + \frac{q}{p} = 3,$

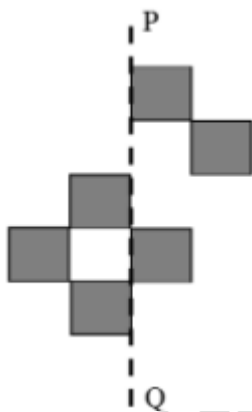
Squaring both sides,

$$\left(\frac{p}{q} + \frac{q}{p}\right)^2 = 3^2$$

$$\frac{p^2}{q^2} + \frac{q^2}{p^2} + 2 = 9$$

$$\frac{p^2}{q^2} + \frac{q^2}{p^2} = 7$$

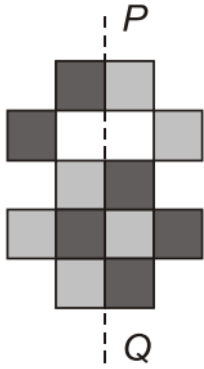
3. The least number of squares that must be added so that the line P-Q becomes the line of symmetry is \_\_\_\_\_.



- (a) 4
- (b) 3
- (c) 6
- (d) 7

Ans. c

Exp:



To make P-Q as symmetric line, the minimum number of black square added = 6.

4. Nostalgia is to anticipation as \_\_\_\_\_ is to \_\_\_\_\_

Which one of the following options maintains a similar logical relation in the above sentence?

- (a) Present, past
- (b) Future, past
- (c) Past, future
- (d) Future, present

Ans. c

Exp:

Nostalgia refers to a feeling, fondness and slight sadness thinking of past and anticipate is to predicting future.

5. Consider the following sentences:

- (i) I woke up from sleep.
- (ii) I woked up from sleep.
- (iii) I was woken up from sleep.
- (iv) I was wokened up from sleep.

Which of the above sentences are grammatically CORRECT?

- (a) (i) and (ii)
- (b) (i) and (iii)
- (c) (ii) and (iii)

(d) (i) and (iv)

Ans. b

Exp:

Wake – Woke – Woken are three form of the verb.

**Q. 6 – Q. 10 Multiple Choice Question (MCQ), carry TWO marks each (for each wrong answer: – 2/3).**

6 Given below are two statements and two conclusions.

Statement 1: All purple are green.

Statement 2: All black are green.

Conclusion I: Some black are purple.

Conclusion II: No black is purple.

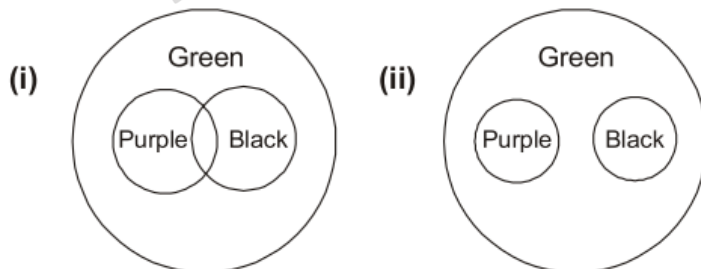
Based on the above statements and conclusions, which one of the following options is logically CORRECT?

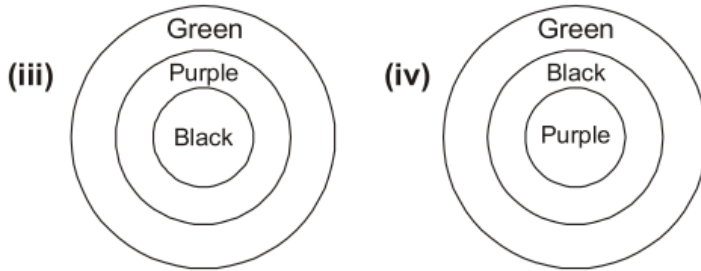
- (a) Only conclusion I is correct.
- (b) Only conclusion II is correct.
- (c) Either conclusion I or II is correct.
- (d) Both conclusion I and II are correct.

Ans. c

Exp:

Possible cases can be,





7. Computers are ubiquitous. They are used to improve efficiency in almost all fields from agriculture to space exploration. Artificial intelligence (AI) is currently a hot topic. AI enables computers to learn, given enough training data. For humans, sitting in front of a computer for long hours can lead to health issues.

Which of the following can be deduced from the above passage?

- (i) Nowadays, computers are present in almost all places.
- (ii) Computers cannot be used for solving problems in engineering.
- (iii) For humans, there are both positive and negative effects of using computers.
- (iv) Artificial intelligence can be done without data.

- (a) (ii) and (iii)
- (b) (ii) and (iv)
- (c) (i), (iii) and (iv)
- (d) (i) and (iii)

Ans. d

Exp:

Ubiquitous is the keyword to justify option (i). Positive and negative effect for humans justifies option (iii).

8. Consider a square sheet of side 1 unit. In the first step, it is cut along the main diagonal to get two triangles. In the next step, one of the cut triangles is revolved about its short edge to form a solid cone. The volume of the resulting cone, in cubic units, is \_\_\_\_\_

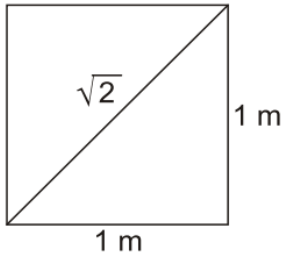
- (a)  $\frac{\pi}{3}$
- (b)  $\frac{2\pi}{3}$

(c)  $\frac{3\pi}{2}$

(d)  $3\pi$

Ans. a

Exp:

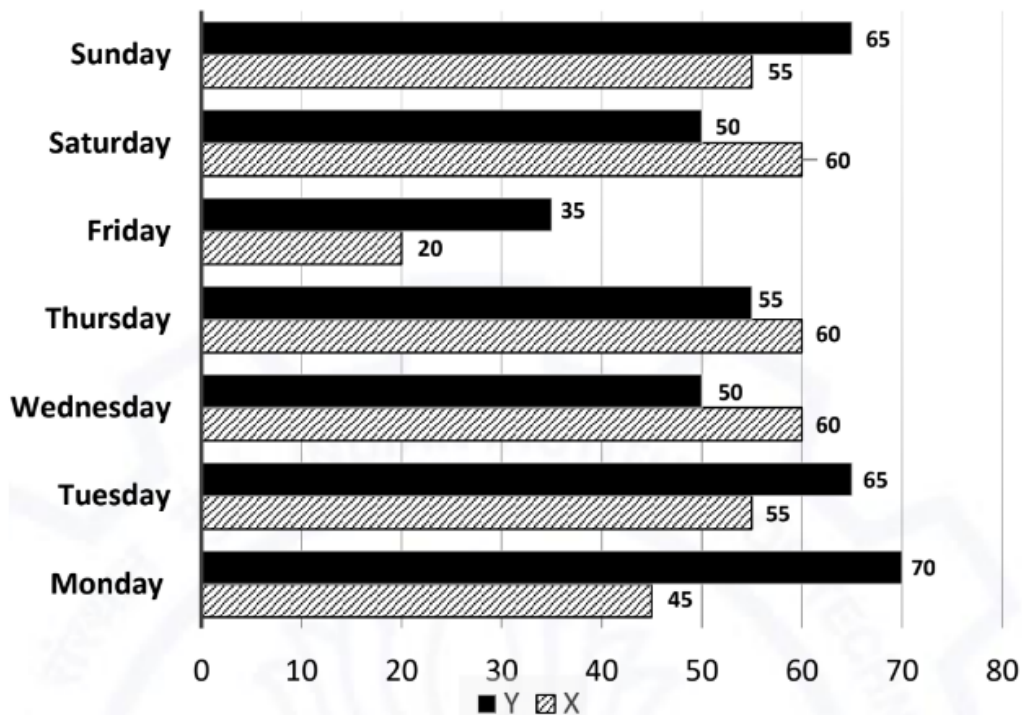


One of the triangle is revolved about its short side, resulting a cone.

Hence,  $r = 1$ ,  $H = 1$

Volume of cone,  $V = \frac{1}{3} \pi r^2 H = \frac{\pi}{3}$

9. The number of minutes spent by two students, X and Y, exercising every day in a given week are shown in the bar chart below.



The number of days in the given week in which one of the students spent a minimum of 10% more than the other student, on a given day, is

(a) 4

(b) 5

(c) 6

(d) 7

Ans. c

Exp:

$$\text{On Sunday, the \%} = \frac{65-55}{55} \times 100 = 18.18\%$$

$$\text{On Saturday, the \%} = \frac{60-50}{50} \times 100 = 20\%$$

$$\text{On Friday, the \%} = \frac{35-20}{20} \times 100 = 75\%$$

$$\text{On Thursday, the \%} = \frac{60-55}{55} \times 100 = 9.09\%$$

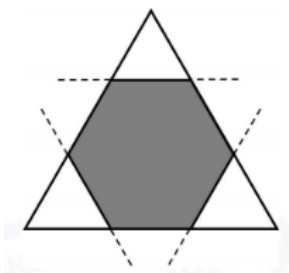
$$\text{On Wednesday, the \%} = \frac{60-50}{50} \times 100 = 20\%$$

$$\text{On Tuesday, the \%} = \frac{65-55}{55} \times 100 = 18.18\%$$

$$\text{On Monday, the \%} = \frac{70-45}{45} \times 100 = 55.56\%$$

Total six days are there when one of the students spent a minimum of 10% more than the other students.

10. Corners are cut from an equilateral triangle to produce a regular convex hexagon as shown in the figure below.



The ratio of the area of the regular convex hexagon to the area of the original equilateral triangle is

(a) 2 : 3

(b) 3 : 4

(c) 4 : 5

(d) 5 : 6

Ans. a

Exp:

Let the side of the two larger equilateral triangle = a

Then side of regular hexagon =  $\frac{a}{3}$

Area of regular Hexagon =  $6 \times \frac{\sqrt{3}}{4} \left(\frac{a}{3}\right)^2$

Area of triangle =  $\frac{\sqrt{3}}{4} (a)^2$

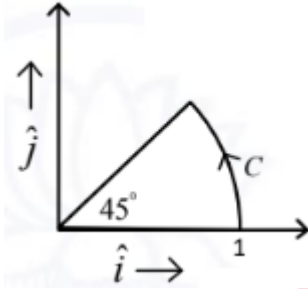
Required ratio =  $6 \times \frac{\sqrt{3}}{4} \left(\frac{a}{3}\right)^2 : \frac{\sqrt{3}}{4} (a)^2 :: 2 : 3$



**Electronics and Communication Engineering (EC)**

**Q.1 – Q.15 Multiple Choice Question (MCQ), carry ONE mark each (for each wrong answer: – 1/3).**

1) The vector function  $F(r) = -x \hat{i} + y \hat{j}$  is defined over a circular arc  $C$  shown in the figure.



The line integral of  $\int_C F(r) \cdot dr$  is

(a)  $\frac{1}{2}$

(b)  $\frac{1}{4}$

(c)  $\frac{1}{6}$

(d)  $\frac{1}{3}$

Ans. a

Exp:

$$F(r) = -x \hat{i} + y \hat{j}$$

$$\int_C \vec{F} \cdot d\vec{r} = \int_C -x dx + y dy$$

$$= \int_{\theta=0}^{45^\circ} (-\cos \theta (-\sin \theta) + \sin \theta \cos \theta) d\theta$$

$$\int_{\theta=0}^{\pi/4} \sin 2\theta d\theta = -\left[ \frac{\cos 2\theta}{2} \right]_0^{\pi/4} = \frac{1}{2}$$

2. Consider the differential equation given below:

$$\frac{dy}{dx} + \frac{x}{1-x^2} y = x\sqrt{y}$$

The integrating factor of the differential equation is

(a)  $(1-x^2)^{-3/4}$

(b)  $(1-x^2)^{-1/4}$

(c)  $(1-x^2)^{-3/2}$

(d)  $(1-x^2)^{-1/2}$

Ans. b

Exp:

$$\frac{dy}{dx} + \frac{x}{1-x^2} y = x\sqrt{y}$$

I. F. = ?

Divided by  $\sqrt{y}$

$$\frac{1}{\sqrt{y}} \frac{dy}{dx} + \frac{x}{1-x^2} \sqrt{y} = x$$

$$2 \frac{du}{dx} + \frac{x}{1-x^2} u = x$$

Let  $x\sqrt{y} = u$

$$\frac{1}{2\sqrt{y}} \frac{dy}{dx} = \frac{du}{dx}$$

$$\Rightarrow \frac{du}{dx} + \frac{x}{2(1-x^2)} u = \frac{x}{2} \rightarrow \text{lines diff. Equ}$$

$$\text{I.F.} = e^{\int \frac{x}{2(1-x^2)} dx} = e^{\frac{-1}{4} \log(1-x^2)} = e^{\log(1-x^2)^{-1/4}}$$

$$\text{I.F.} (1-x^2)^{-1/4}$$

3. Two continuous random variables X and Y are related as

$$Y = 2X + 3$$

Let  $\sigma_X^2$  and  $\sigma_Y^2$  denote the variances of X and Y, respectively. The variances are related as

(a)  $\sigma_Y^2 = 2\sigma_X^2$

(b)  $\sigma_Y^2 = 4\sigma_X^2$

(c)  $\sigma_Y^2 = 5\sigma_X^2$

(d)  $\sigma_Y^2 = 25\sigma_X^2$

Ans. b

Exp:

$$Y = 2X + 3$$

$$\text{Var}[Y] = E[(Y - \bar{Y})^2]$$

$$E[Y] = \bar{Y} = 2\bar{X} + 3$$

$$\text{Var}[Y] = E[(2X + 3 - 2\bar{X} - 3)^2]$$

$$= E[4(X - \bar{X})^2]$$

$$= 4 \cdot E[(X - \bar{X})^2]$$

$$\sigma_Y^2 = 4\sigma_X^2$$

4. Consider a real-valued base-band signal  $x(t)$ , band limited to 10 kHz. The Nyquist rate for the signal  $y(t) = x(t) x\left(1 + \frac{t}{2}\right)$  is

(a) 15 kHz

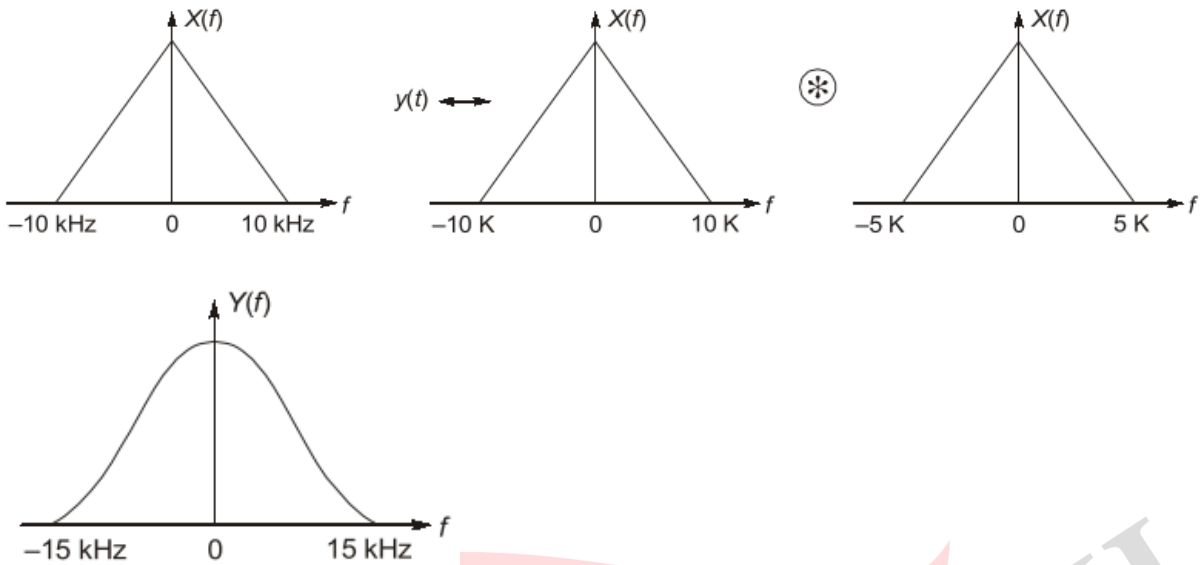
(b) 30 kHz

(c) 60 kHz

(d) 20 kHz

Ans. b

Exp:



$$NR = 2 \times f_{\max} = 2 \times 15 = 30 \text{ kHz}$$

5. Consider two 16-point sequences  $x[n]$  and  $h[n]$ . Let the linear convolution of  $x[n]$  and  $h[n]$  be denoted by  $y[n]$ , while  $z[n]$  denotes the 16-point inverse discrete Fourier transform (IDFT) of the product of the 16-point DFTs of  $x[n]$  and  $h[n]$ . The value(s) of  $k$  for which  $z[k] = y[k]$  is/are

- (a)  $k = 0, 1, 2, \dots, 15$
- (b)  $k = 0$
- (c)  $k = 15$
- (d)  $k = 0$  and  $k = 15$

Ans. c

Exp:

If two 'N' point signals  $x(n)$  and  $h(n)$  are convolving with each other linearly and circularly then,

$$y(k) = z(k) \text{ at } k = N - 1$$

where,  $y(n)$  = Linear convolution of  $x(n)$  and  $h(n)$

$z(n)$  = Circular convolution of  $x(n)$  and  $h(n)$

Since,  $N = 16$  (Given)

Therefore,  $y(k) = z(k)$  at  $k = N - 1 = 15$

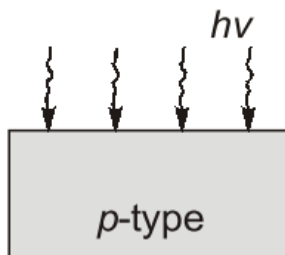
6. A bar of silicon is doped with boron concentration of  $10^{16} \text{ cm}^{-3}$  and assumed to be fully ionized. It is exposed to light such that electron-hole pairs are generated throughout the volume of the bar at the rate of  $10^{20} \text{ cm}^{-3}\text{s}^{-1}$ . If the recombination lifetime is  $100 \mu\text{s}$ , intrinsic carrier concentration of silicon is  $10^{10} \text{ cm}^{-3}$  and assuming 100% ionization of boron, then the approximate product of steady-state electron and hole concentrations due to this light exposure is

- (a)  $10^{20} \text{ cm}^{-6}$   
 (b)  $2 \times 10^{20} \text{ cm}^{-6}$   
 (c)  $10^{32} \text{ cm}^{-6}$   
 (d)  $2 \times 10^{32} \text{ cm}^{-6}$

Ans. d

Exp:

Boron  $\rightarrow$  Acceptor type doping



$$N_A = 10^{16} \text{ cm}^{-3}, g_{op} = 10^{20} \text{ cm}^{-3} \text{ s}^{-1}, \tau = 100 \mu\text{s}, n_i = 10^{10} \text{ cm}^{-3}$$

Product of steady state electron-hole concentration = ?

At thermal equilibrium (before shining light)

$$\text{Hole concentration, } p_o \approx N_A = 10^{16} \text{ cm}^{-3}$$

$$\text{Electron concentration, } n_o = \frac{n_i^2}{p_o} = \frac{10^{20}}{10^{16}} = 10^4 \text{ cm}^{-3}$$

After, illumination of light, hole concentration,  $p = p_o + \delta p$

Electron concentration,  $n = n_o + \delta n$

Due to shining light, excess carrier concentration,

$$\delta p = \delta n = g_{op} \cdot \tau = 10^{20} \times 100 \times 10^{-6} = 10^{16} \text{ cm}^{-3}$$

$$\therefore p = 10^{16} + 10^{16} = 2 \times 10^{16} \text{ cm}^{-3}$$

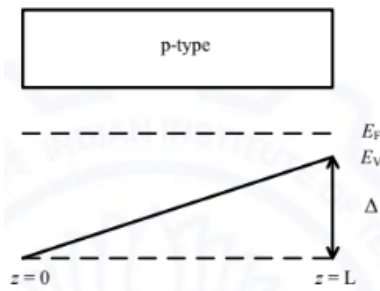
$$n = 10^4 + 10^{16} \approx 10^{16} \text{ cm}^{-3}$$

So, product of steady state electron – hole concentration

$$= np = 10^{16} \times 2 \times 10^{16} = 2 \times 10^{32} \text{ cm}^{-6}$$

7. The energy band diagram of a p-type semiconductor bar of length L under equilibrium condition (i.e., the Fermi energy level  $E_F$  is constant) is shown in the figure. The valance band EV is sloped

since doping is non-uniform along the bar. The difference between the energy levels of the valence band at the two edges of the bar is  $\Delta$ .



If the charge of an electron is  $q$ , then the magnitude of the electric field developed inside this semiconductor bar is

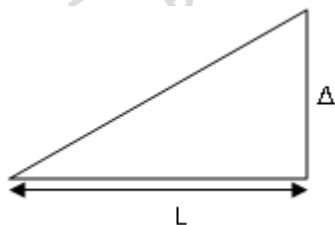
- (a)  $\frac{\Delta}{qL}$
- (b)  $2 \frac{\Delta}{qL}$
- (c)  $\frac{\Delta}{2qL}$
- (d)  $3 \frac{\Delta}{2qL}$

Ans. a

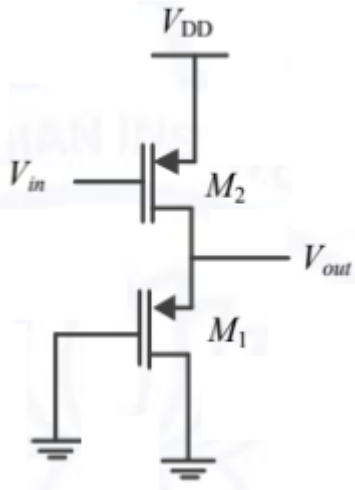
Exp:

The built-in electric field is due to non-uniform doping (the semiconductor is under equilibrium).

$$E = \frac{1}{q} \frac{dE_v}{dx} = \frac{1}{q} \frac{\Delta}{L}$$



8. In the circuit shown in the figure, the transistors  $M_1$  and  $M_2$  are operating in saturation. The channel length modulation coefficients of both the transistors are non-zero. The transconductance of the MOSFETs  $M_1$  and  $M_2$  are  $g_{m1}$  and  $g_{m2}$ , respectively, and the internal resistance of the MOSFETs  $M_1$  and  $M_2$  are  $r_{o1}$  and  $r_{o2}$ , respectively.



Ignoring the body effect, the ac small signal voltage gain ( $\partial V_{out} / \partial V_{in}$ ) of the circuit is

(a)  $-g_{m2}(r_{o1} \parallel r_{o2})$

(b)  $-g_{m2} \left( \frac{1}{g_{m1}} \parallel r_{o2} \right)$

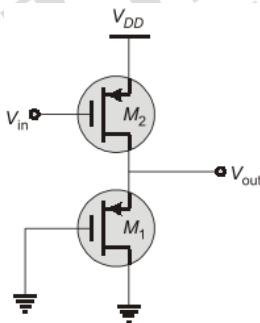
(c)  $-g_{m1} \left( \frac{1}{g_{m2}} \parallel r_{o1} \parallel r_{o2} \right)$

(d)  $-g_{m2} \left( \frac{1}{g_{m1}} \parallel r_{o1} \parallel r_{o2} \right)$

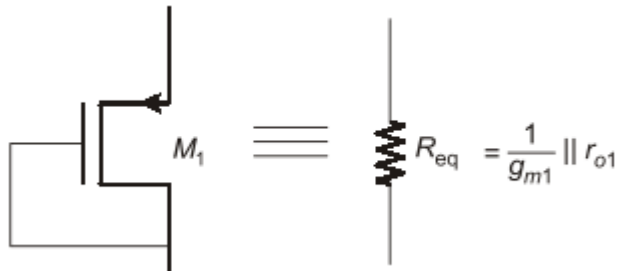
Ans. d

Exp:

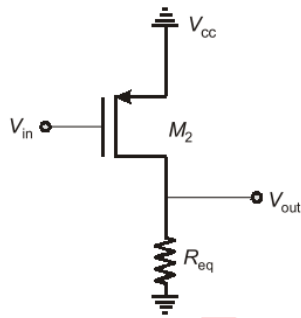
MOSFET  $M_2$  acts as common source amplifier.



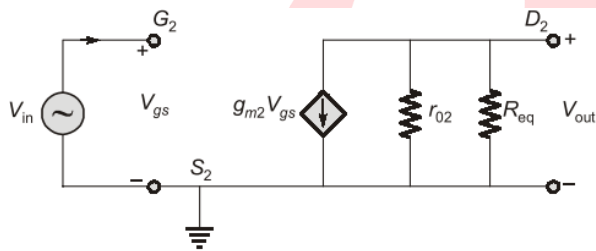
Drain to gate connected MOSFET  $M_1$  acts as load.



For given circuit, AC equivalent is as shown.



Replace  $M_2$  with small signal model.

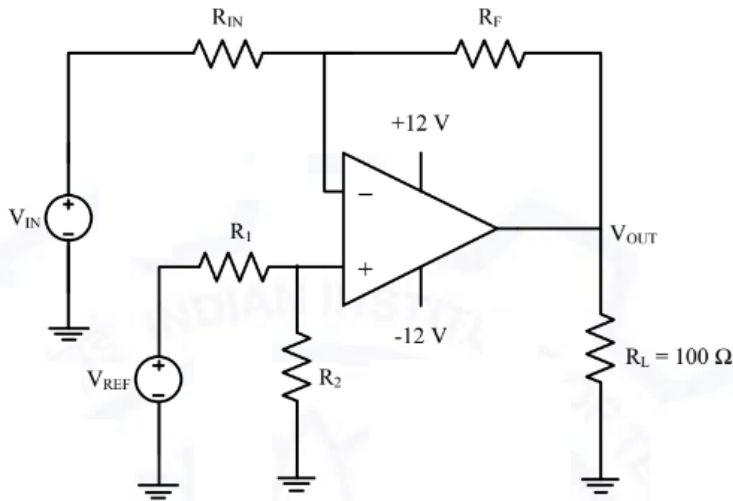


$$\frac{V_{out}}{V_{in}} = \frac{-g_{m2} V_{gs} (r_{o2} \parallel R_{eq})}{V_{gs}}$$

$$A_v = -g_{m2} \left( \frac{1}{g_{m1}} \parallel r_{o1} \parallel r_{o2} \right)$$

9. For the circuit with an ideal OPAMP shown in the figure,  $V_{REF}$  is fixed.





If  $V_{OUT} = 1$  volt for  $V_{IN} = 0.1$  volt and  $V_{OUT} = 6$  volt for  $V_{IN} = 1$  volt, where  $V_{OUT}$  is measured across  $R_L$  connected at the output of this OPAMP, the value of  $R_F/R_{IN}$  is

- (a) 3.285
- (b) 2.860
- (c) 3.825
- (d) 5.555

Ans. d

Exp:

$$V^- = V^+$$

$$\frac{V_{out} R_{in} + V_{in} R_F}{R_{in} + R_F} = \frac{V_{ref} R_2}{R_1 + R_2}$$

$$\frac{1 \times R_{in} + 0.1 \times R_F}{R_{in} + R_F} = \frac{V_{ref} R_2}{R_1 + R_2} \quad (i)$$

$$\frac{6 \times R_{in} + 1 \times R_F}{R_{in} + R_F} = \frac{V_{ref} R_2}{R_1 + R_2} \quad (ii)$$

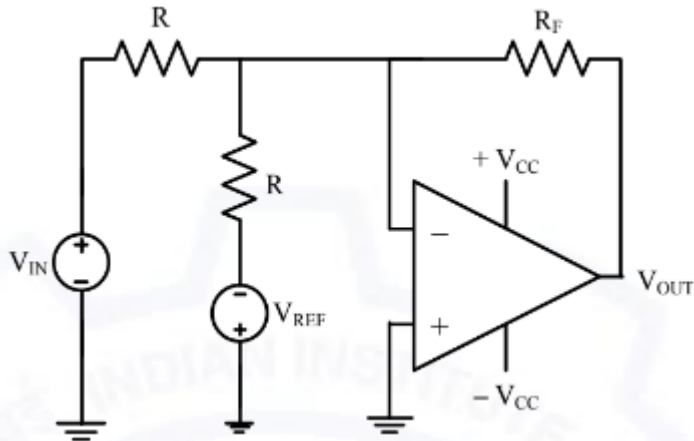
From (i) & (ii)

$$1 \times R_{in} + 0.1 \times R_F = 6 \times R_{in} + 1 \times R_F$$

$$-5 R_{in} = 0.9 R_F$$

$$\therefore \frac{R_F}{R_{in}} = -5.55 \quad (\text{According to the given data magnitude is taken})$$

10. Consider the circuit with an ideal OPAMP shown in the figure.



Assuming  $|V_{IN}| \ll |V_{CC}|$  and  $|V_{REF}| \ll |V_{CC}|$ , the condition at which  $V_{OUT}$  equals to zero is

- (a)  $V_{IN} = V_{REF}$
- (b)  $V_{IN} = 0.5 V_{REF}$
- (c)  $V_{IN} = 2 V_{REF}$
- (d)  $V_{IN} = 2 + V_{REF}$

Ans. a

Exp:

For ideal op-amp,  $V^- = V^+ = 0$

KCL at node  $V^-$  :

$$\frac{V_{in} - 0}{R} + \frac{(-V_{ref} - 0)}{R} + \frac{V_{out} - 0}{R_F} = 0$$

$$\frac{V_{out}}{R_F} = \frac{1}{R}(V_{ref} - V_{in})$$

$$V_{out} = \frac{R_F}{R}(V_{ref} - V_{in})$$

We want,  $V_{out} = 0$

$$\Rightarrow V_{ref} - V_{in} = 0$$

$$\therefore V_{IN} = V_{REF}$$

11. If  $(1235)_x = (3033)_y$ , where  $x$  and  $y$  indicate the bases of the corresponding numbers, then

- (a)  $x = 7$  and  $y = 5$
- (b)  $x = 8$  and  $y = 6$
- (c)  $x = 6$  and  $y = 4$
- (d)  $x = 9$  and  $y = 7$

Ans. b

Exp:

$$x^3 + 2x^2 + 3x + 5 = 3y^3 + 3y + 3$$

Option (b) will satisfy the equation.

12. Addressing of a  $32K \times 16$  memory is realized using a single decoder. The minimum number of AND gates required for the decoder is

- (a)  $2^8$
- (b)  $2^{32}$
- (c)  $2^{15}$
- (d)  $2^{19}$

Ans. c

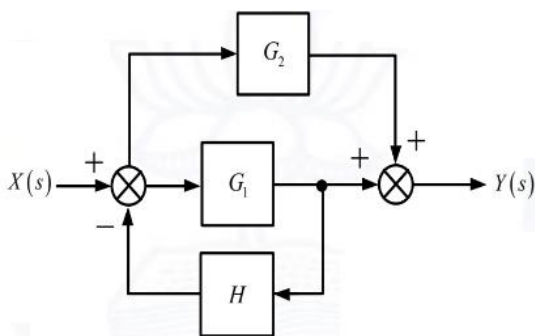
Exp:

For  $N \times 2^N$ , decoder, there are  $2^N$  AND gates required at output.

$$\therefore 32K \times 16 = 2^5 \times 2^{10} \times 16 = 2^{15} \times 16$$

$\therefore 2^{15}$  AND gates required to realize the given memory address.

13. The block diagram of a feedback control system is shown in the figure.



The transfer function  $\frac{Y(s)}{X(s)}$  of the system is

(a)  $\frac{G_1 + G_2 + G_1 G_2 H}{1 + G_1 H}$

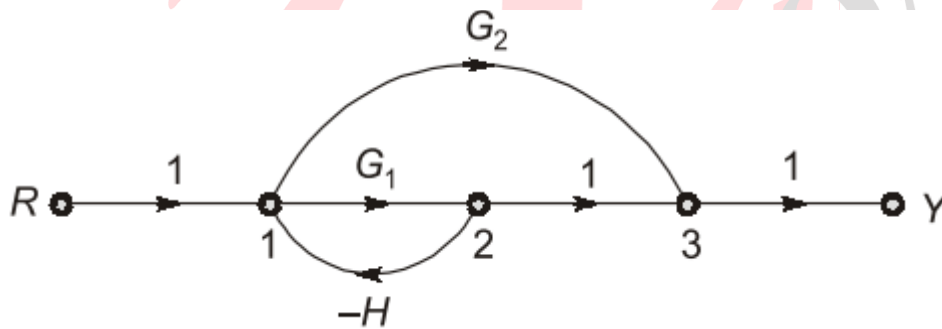
(b)  $\frac{G_1 + G_2}{1 + G_1 H + G_2 H}$

(c)  $\frac{G_1 + G_2}{1 + G_1 H}$

(d)  $\frac{G_1 + G_2 + G_1 G_2 H}{1 + G_1 H + G_2 H}$

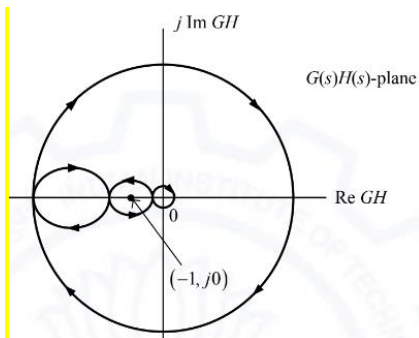
Ans. c

Exp:



$$\frac{Y}{R} = \frac{G_1(1-0) + G_2(1-0)}{1 - [-G_1 H]} = \frac{G_1 + G_2}{1 + G_1 H}$$

14. The complete Nyquist plot of the open-loop transfer function  $G(s)H(s)$  of a feedback control system is shown in the figure.



If  $G(s)H(s)$  has one zero in the right-half of the  $s$ -plane, the number of poles that the closed-loop system will have in the right-half of the  $s$ -plane is

(a) 0

(b) 1

(c) 4

(d) 3

Ans. d

Exp:

Nquist plot is not matched according to given data.

15. Consider a rectangular coordinate system (x, y, z) with unit vectors  $a_x$ ,  $a_y$ , and  $a_z$ . A plane wave travelling in the region  $z \geq 0$  with electric field vector  $E = 10 \cos(2 \times 10^8 t + \beta z) a_y$  is incident normally on the plane at  $z = 0$ , where  $\beta$  is the phase constant. The region  $z \geq 0$  is in free space and the region  $z < 0$  is filled with a lossless medium (permittivity  $\epsilon = \epsilon_0$ , permeability  $\mu = 4\mu_0$ , where  $\epsilon_0 = 8.85 \times 10^{-12}$  F/m and  $\mu_0 = 4\pi \times 10^{-7}$  H/m). The value of the reflection coefficient is

(a)  $\frac{1}{3}$

(b)  $\frac{3}{5}$

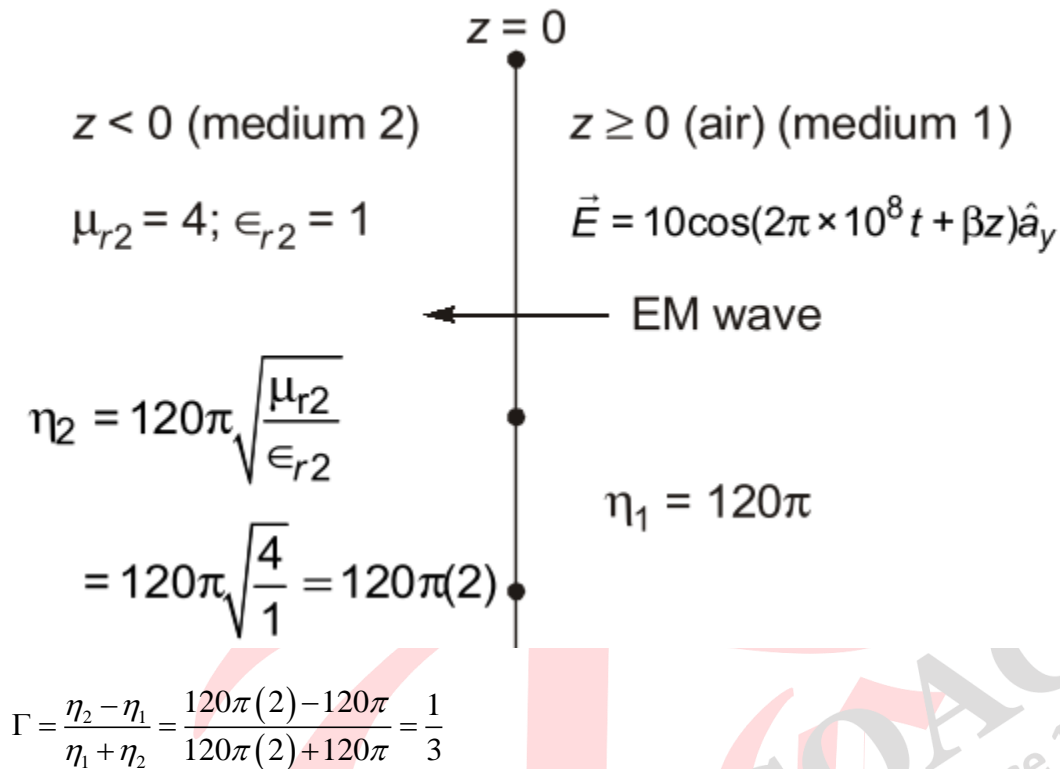
(c)  $\frac{2}{5}$

(d)  $\frac{2}{3}$

Ans. a

Exp:

Given  $\vec{E} = 10 \cos(2\pi \times 10^8 t + \beta z) \hat{a}_y$ , for  $z \geq 0$  having free space. For  $z < 0$  medium has  $\epsilon_r = 1$  ;  
 $\mu_r = 4$



**Q.16 – Q.25 Numerical Answer Type (NAT), carry ONE mark each (no negative marks).**

16. If the vectors  $(1, 0, -1, 0, 2, 0)$ ,  $(7, 0, 3, 0, x)$  and  $(2, 0, 3, 0, 1, 0)$  in  $\mathbb{R}^3$  are linearly dependent, the value of  $x$  is \_\_\_\_\_

Ans. 8.0

Exp:

$(1, -1, 2)$

$(7, 3, x)$  are linearly dependent when  $x = ?$

$(2, 3, 1)$

$$\begin{vmatrix} 1 & -1 & 2 \\ 7 & 3 & x \\ 2 & 3 & 1 \end{vmatrix} = 0$$

$$1(3 - 3x) + 1(7 - 2x) + 2(15) = 0$$

$$\therefore x = 8$$

17. Consider the vector field  $F = a_x(4y - c_1z) + a_y(4x + 2z) + a_z(2y + z)$  in a rectangular coordinate system  $(x, y, z)$  with unit vectors  $a_x, a_y,$  and  $a_z$ . If the field  $F$  is irrotational (conservative), then the constant  $c_1$  (in integer) is \_\_\_\_\_

Ans. 0

Exp:

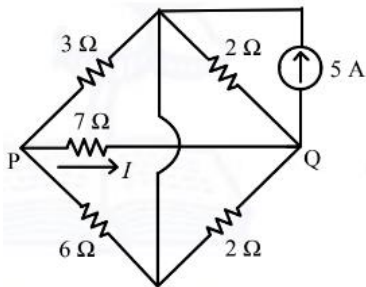
$$\nabla \times \vec{F} = 0$$

$$\begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 4y - c_1z & 4x + 2z & 2y + z \end{vmatrix} = 0$$

$$= i(2 - 2) - j(0 + c_1) + k(4 - 4) = 0$$

$$c_1 = 0$$

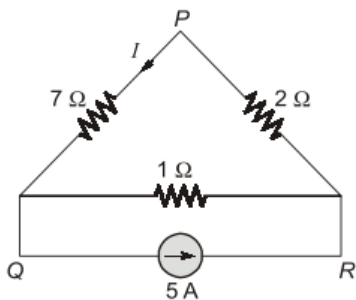
18. Consider the circuit shown in the figure.



The current  $I$  flowing through the  $7\ \Omega$  resistor between  $P$  and  $Q$  (rounded off to one decimal place) is \_\_\_\_\_ A.

Ans. 0.5

Exp:



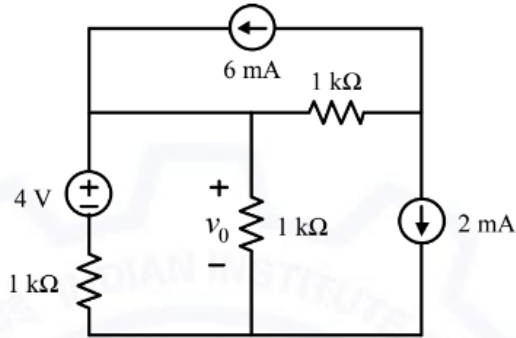
Redraw the circuit,

$$3\ \Omega \parallel 6\ \Omega = 2\ \Omega$$

$$2 \Omega || 2 \Omega = 1 \Omega$$

$$I = 5 \times \frac{1}{10} = 0.5 \text{ A}$$

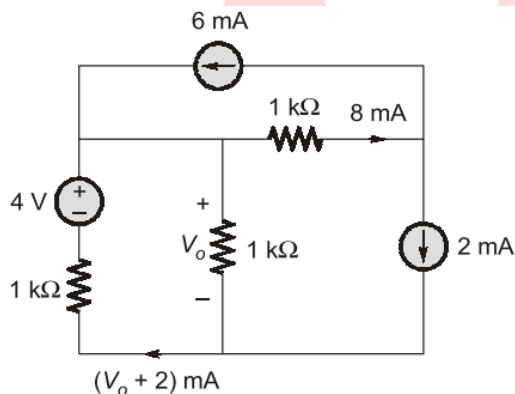
19. Consider the circuit shown in the figure.



The value of  $v_o$  (rounded off to one decimal place) is \_\_\_\_\_ V.

Ans. 1.0

Exp:



Apply KVL equation in first loop, we get

$$V_o - 4 + 1(V_o + 2) = 0$$

$$V_o = 1 \text{ V}$$

20. An 8-bit unipolar (all analog output values are positive) digital-to-analog converter (DAC) has a full-scale voltage range from 0 V to 7.68 V. If the digital input code is 10010110 (the leftmost bit is MSB), then the analog output voltage of the DAC (rounded off to one decimal place) is \_\_\_\_\_ V.

Ans. 4.5

Exp:

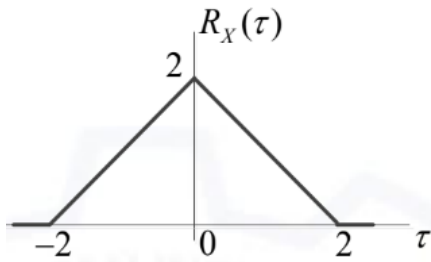


Given:  $V_{FS} = 7.68 \text{ V}$ ,  $n = 8 \text{ bit}$

$$\text{Resolution (k)} = \frac{V_{FS}}{2^n - 1} = 0.03$$

Now,  $V_{DAC} = k \times [\text{Decimal equivalent}] = 0.03 \times 150 = 4.5 \text{ V}$

21. The autocorrelation function  $R_X(\tau)$  of a wide-sense stationary random process  $X(t)$  is shown in the figure.



The average power of  $X(t)$  is \_\_\_\_\_

Ans. 2.0

Exp:

Average power  $[X(t)] = R_X(0) = 2$

22. Consider a carrier signal which is amplitude modulated by a single-tone sinusoidal message signal with a modulation index of 50%. If the carrier and one of the sidebands are suppressed in the modulated signal, the percentage of power saved (rounded off to one decimal place) is \_\_\_\_\_

Ans. 94.2 – 94.6

Exp:

If carrier and one of the sidebands are suppressed, then % of power saved

$$= \frac{\text{Power saved}}{\text{Total power}} = \frac{P_c + \frac{P_c \mu^2}{4}}{P_c \left[ 1 + \frac{\mu^2}{2} \right]} = \frac{4 + \mu^2}{4 + 2\mu^2}$$

$$= 94.4 \% \quad (\mu = 0.5)$$

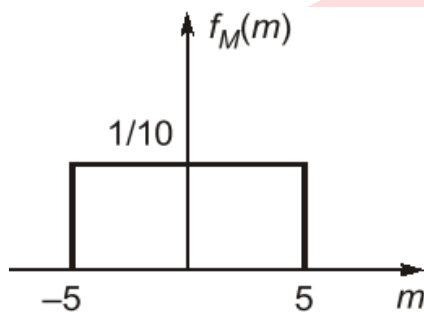
23. A speech signal, band limited to 4 kHz, is sampled at 1.25 times the Nyquist rate. The speech samples, assumed to be statistically independent and uniformly distributed in the range  $-5$  V to  $+5$  V, are subsequently quantized in an 8-bit uniform quantizer and then transmitted over a voice-grade AWGN telephone channel. If the ratio of transmitted signal power to channel noise power is 26 dB, the minimum channel bandwidth required to ensure reliable transmission of the signal with arbitrarily small probability of transmission error (rounded off to two decimal places) is \_\_\_\_\_ kHz.

Ans. 9.24 – 9.28

Exp:

$$f_m = 4 \text{ kHz}$$

$$f_s = 1.25 \text{ NR} = 1.25 \times (2f_m) = 10 \text{ kHz}$$



$$n = 8 \text{ bits/sample and } \frac{S}{N} = 26 \text{ dB} = 10^{2.6}$$

For arbitrarily small probability of transmission error,

$$C \geq R_b \Rightarrow B \log_2 \left( 1 + \frac{S}{N} \right) \geq n f_s$$

$$B \log_2 (1 + 10^{2.6}) \geq 8 \times 10 \text{ K} \Rightarrow B \geq 9.25 \text{ kHz}$$

$$B_{\min} = 9.25 \text{ kHz}$$

24. A 4 kHz sinusoidal message signal having amplitude 4 V is fed to a delta modulator (DM) operating at a sampling rate of 32 kHz. The minimum step size required to avoid slope overload noise in the DM (rounded off to two decimal places) is \_\_\_\_\_ V.

Ans. 3.12 – 3.16

Exp:

$$f_m = 4 \text{ kHz}, A_m = 4 \text{ V}, f_s = 32 \text{ kHz}$$

To avoid SOE  $\rightarrow \frac{\Delta}{T_s} \geq 2\pi f_m A_m$

$\Delta \times 32 \text{ k} \geq 2\pi \times 4 \text{ k} \times 4 \text{ V}$

$\Delta \geq \pi$

$(\Delta)_{\min} = \pi \text{ volts} = 3.14 \text{ volts}$

25. The refractive indices of the core and cladding of an optical fiber are 1.50 and 1.48, respectively. The critical propagation angle, which is defined as the maximum angle that the light beam makes with the axis of the optical fiber to achieve the total internal reflection, (rounded off to two decimal places) is \_\_\_\_\_ degree.

Ans. 9.30 – 9.44

Exp:

Given that

Refractive index of core  $\eta_1 = 1.50$ , Refractive index of clad  $\eta_2 = 1.48$

Critical propagation angle ( $\theta_a$ )

$$\theta_a = \sin^{-1} \left[ \sqrt{\eta_1^2 - \eta_2^2} \right] = \sin^{-1} \left[ \sqrt{1.5^2 - 1.48^2} \right] = 14.13$$

26. Consider the integral

$$\oint_C \frac{\sin(x)}{x^2(x^2+4)} dx$$

where C is a counter-clockwise oriented circle defined as  $|x - i| = 2$ . The value of the integral is

(a)  $-\frac{\pi}{8} \sin(2i)$

(b)  $\frac{\pi}{8} \sin(2i)$

(c)  $-\frac{\pi}{4} \sin(2i)$

(d)  $\frac{\pi}{4} \sin(2i)$

Ans. a

Exp:

$$\oint_C \frac{\sin(x)}{x^2(x^2+4)} dx, \quad c : |x-i| = 2$$

Poles are given by  $x^2 = 0$  and  $x^2 + 4 = 0$

$\Rightarrow x = 0$  is a pole of order '2'

$x = 2i$  are simple nodes

$x = 0$  lies inside 'c',  $x = 2i$  lies inside 'c',  $x = -2i$  lies outside 'c'

$$Res_0 = \frac{1}{(2-1)} \lim_{x \rightarrow 0} \frac{d}{dz} \left[ (x-0)^2 \frac{\sin x}{x^2(x^2+4)} \right] = \lim_{x \rightarrow 0} \frac{(x^2+4)\cos x - \sin x(2x)}{(x^2+4)^2} = \frac{1}{4}$$

$$Res_{2i} = \lim_{x \rightarrow 2i} (x-2i) \frac{\sin x}{x^2(x-2i)(x+2i)} = \frac{\sin(2i)}{(-4)(4i)}$$

$$\text{By CRT } \oint_C f dx = 2\pi i [Res_0 + Res_{2i}] = 2\pi i \left[ \frac{1}{4} + \frac{\sin(2i)}{-16} \right]$$

27. A box contains the following three coins.

I. A fair coin with head on one face and tail on the other face.

II. A coin with heads on both the faces.

III. A coin with tails on both the faces.

A coin is picked randomly from the box and tossed. Out of the two remaining coins in the box, one coin is then picked randomly and tossed. If the first toss results in a head, the probability of getting a head in the second toss is

(a)  $\frac{2}{5}$

(b)  $\frac{1}{3}$

(c)  $\frac{1}{2}$

(d)  $\frac{2}{3}$

Ans. b

Exp:

Let  $P(H_2)$  = Probability of getting head in second toss

$P(H_1)$  = Probability of getting head in first toss

$$P\left(\frac{H_2}{H_1}\right) = \frac{P(H_2 \cap H_1)}{P(H_1)}$$

$$P(H_1) = \frac{1}{3} \times \frac{1}{2} + \frac{1}{3} \times 1 + \frac{1}{3} \times 0 = \frac{1}{2}$$

To get head in second toss when head came in first toss, following cases can be made

**1. Fair coin :**

$$\text{Both head coin} = \frac{1}{3} \times \frac{1}{2} \times \frac{1}{2} \times 1 = \frac{1}{12}$$

$$\text{Both tail coin} = \frac{1}{3} \times \frac{1}{2} \times \frac{1}{2} \times 0 = 0$$

**2. Both head coin :**

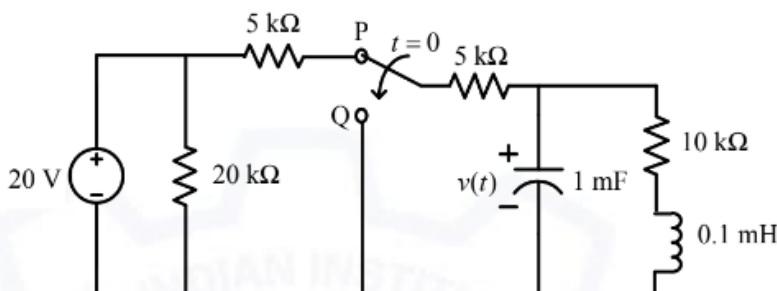
$$\text{Fair coin} = \frac{1}{3} \times 1 \times \frac{1}{2} \times \frac{1}{2} = \frac{1}{12}$$

Both tail coin = 0

$$\therefore P(H_2 \cap H_1) = \frac{1}{12} + \frac{1}{12} = \frac{1}{6}$$

$$P(H_2/H_1) = \frac{1/6}{1/2} = \frac{1}{3}$$

28. The switch in the circuit in the figure is in position P for a long time and then moved to position Q at time  $t = 0$ .



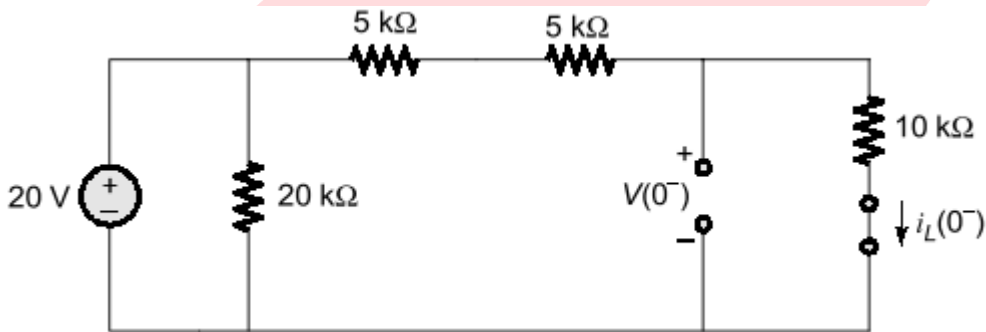
The value of  $\frac{dv(t)}{dt}$  at  $t = 0^+$  is

- (a) 0 V/s
- (b) 3 V/s
- (c) -3 V/s
- (d) -5 V/s

Ans. c

Exp:

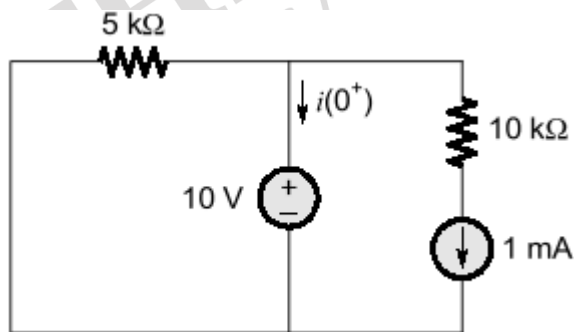
Inductor and capacitors are connected to the inductance source for a long time, so these elements have reached steady state.



$$i_L(0^-) = \frac{20}{5k\Omega + 5k\Omega + 10k\Omega} = 1\text{mA}$$

$$V(0^-) = 10\text{V}$$

$t = 0^+$



$$i(0^+) + \frac{10}{5k} + 1\text{mA} = 0$$

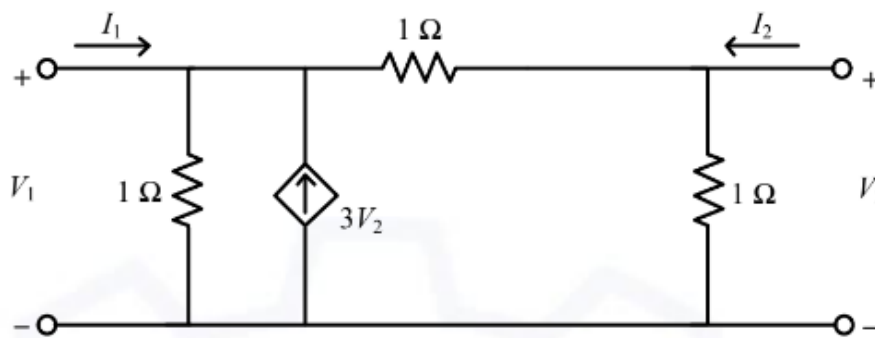
$$i(0^+) = -3\text{mA}$$

$$C \frac{dV(0^+)}{dt} = -3 \text{ mA}$$

$$1 \times 10^{-3} \frac{dV(0^+)}{dt} = -3 \text{ mA}$$

$$\frac{dV(0^+)}{dt} = -3 \text{ V/s}$$

29. Consider the two-port network shown in the figure.

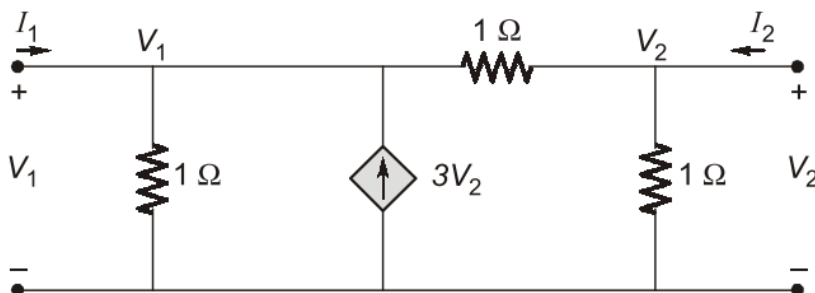


The admittance parameters, in siemens, are

- (a)  $y_{11} = 2, y_{12} = -4, y_{21} = -4, y_{22} = 2$
- (b)  $y_{11} = 1, y_{12} = -2, y_{21} = -1, y_{22} = 3$
- (c)  $y_{11} = 2, y_{12} = -4, y_{21} = -1, y_{22} = 2$
- (d)  $y_{11} = 2, y_{12} = -4, y_{21} = -4, y_{22} = 3$

Ans. c

Exp:



Write KCL at  $V_1$

$$I_1 = \frac{V_1}{1} + \frac{V_1 - V_2}{1} - 3V_2$$

$$I_1 = 2V_1 - 4V_2 \quad (i)$$

Write KCL at  $V_2$

$$I_2 = \frac{V_2}{1} + \frac{V_2 - V_1}{1}$$

$$I_2 = -V_1 + 2V_2 \quad (ii)$$

$$[y] = \begin{bmatrix} 2 & -4 \\ -1 & 2 \end{bmatrix} \square$$

30. For an n-channel silicon MOSFET with 10 nm gate oxide thickness, the substrate sensitivity ( $\partial V_T / \partial |V_{BS}|$ ) is found to be 50 mV/V at a substrate voltage

$|V_{BS}| = 2$  V, where  $V_T$  is the threshold voltage of the MOSFET. Assume that,  $|V_{BS}| \gg 2\phi_B$ , where  $q\phi_B$  is the separation between the Fermi energy level  $E_F$  and the intrinsic level  $E_i$  in the bulk. Parameters given are

Electron charge ( $q$ ) =  $1.6 \times 10^{-19}$  C

Vacuum permittivity ( $\epsilon_0$ ) =  $8.85 \times 10^{-12}$  F/m

Relative permittivity of silicon ( $\epsilon_{Si}$ ) = 12

Relative permittivity of oxide ( $\epsilon_{ox}$ ) = 4

The doping concentration of the substrate is

(a)  $7.37 \times 10^{15} \text{ cm}^{-3}$

(b)  $4.37 \times 10^{15} \text{ cm}^{-3}$

(c)  $2.37 \times 10^{15} \text{ cm}^{-3}$

(d)  $9.37 \times 10^{15} \text{ cm}^{-3}$

Ans. a

Exp:

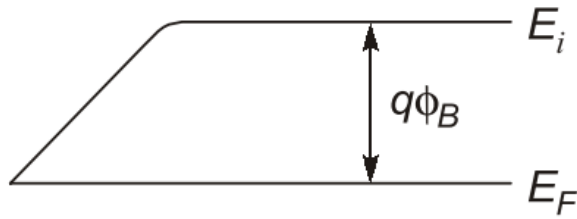
Given, N-channel MOSFET

$$t_{ox} = 10 \text{ nm} = 10 \times 10^{-7} \text{ cm}$$

$$\frac{\partial V_T}{\partial |V_{BS}|} = 50 \text{ mV/V}, \quad |V_{BS}| = 2 \text{ V}$$

$$q = 1.6 \times 10^{-19} \text{ C}, \quad |V_{BS}| \gg 2\phi_B$$





$$\epsilon_0 = 8.85 \times 10^{-12} \text{ F/m} = 8.85 \times 10^{-14} \text{ F/cm}$$

$$\epsilon_{\text{rsi}} = 12$$

$$\epsilon_{\text{rox}} = 4$$

Threshold voltage, including body effect,

$$V_T = \phi_{ms} + \frac{\sqrt{2 \epsilon_{Si} q N_A (2\phi_B - V_{BS})}}{C_{Ox}} + 2\phi_B$$

In question, we need,  $|V_{SB}| = |V_{BS}|$

$$\therefore V_T = \phi_{ms} + \frac{\sqrt{2 \epsilon_{Si} q N_A (2\phi_B + V_{SB})}}{C_{Ox}} + 2\phi_B$$

$$\Rightarrow V_T = \phi_{ms} + \frac{\sqrt{2 \epsilon_{Si} q N_A (2\phi_B + |V_{SB}|)}}{C_{Ox}} + 2\phi_B$$

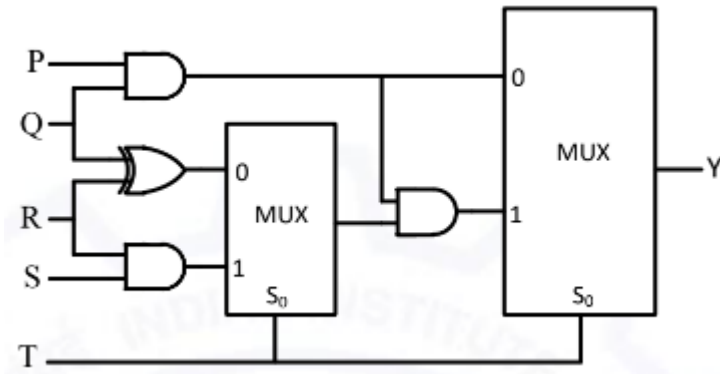
$$\therefore \frac{\partial V_T}{\partial |V_{BS}|} = 0 + \frac{\sqrt{2 \epsilon_{Si} q N_A}}{C_{Ox}} \times \frac{1}{2\sqrt{2\phi_B + |V_{SB}|}} + 0$$

$$\Rightarrow 50 \times 10^{-3} = \frac{\sqrt{2 \times 8.85 \times 10^{-14} \times 12 \times 1.6 \times 10^{-19} N_A}}{\epsilon_{ox}/t_{ox}} \times \frac{1}{2\sqrt{|V_{SB}|}}$$

$$\left( \frac{50 \times 10^{-3} \times 4 \times 8.85 \times 10^{-14}}{10 \times 10^{-7}} \right)^2 = \frac{2 \times 8.85 \times 10^{-14} \times 12 \times 1.6 \times 10^{-19}}{4 \times 2} \quad [\because |V_{SB}| \gg 2\phi_B]$$

$$N_A = 7.37 \times 10^5 \text{ cm}^{-3}$$

31. The propagation delays of the XOR gate, AND gate and multiplexer (MUX) in the circuit shown in the figure are 4 ns, 2 ns and 1 ns, respectively.



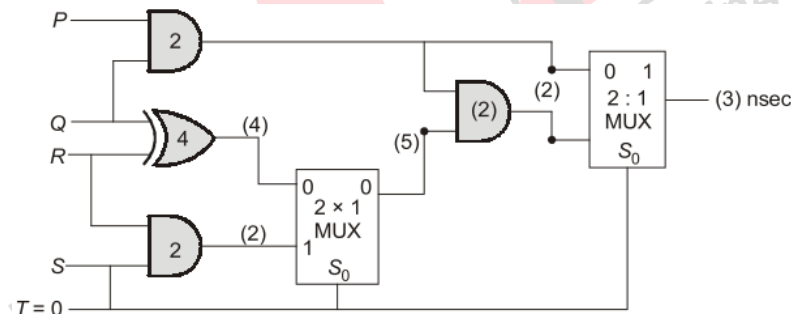
If all the inputs P, Q, R, S and T are applied simultaneously and held constant, the maximum propagation delay of the circuit is

- (a) 3 ns
- (b) 5 ns
- (c) 6 ns
- (d) 7 ns

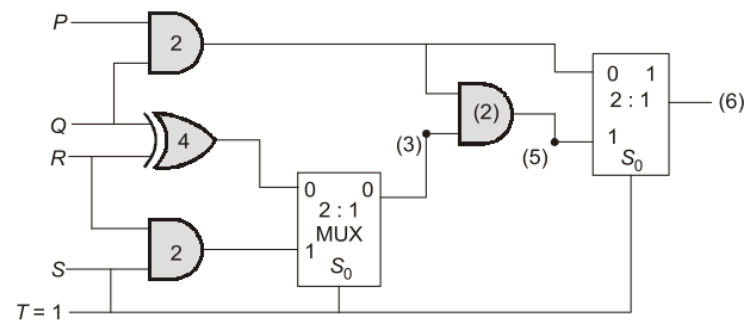
Ans. c

Exp:

For T = 0



For T = 1



∴ Maximum propagation delay for the circuit is 6ns.

32. The content of the registers are  $R_1 = 25H$ ,  $R_2 = 30H$  and  $R_3 = 40H$ . The following machine instructions are executed.

PUSH{ $R_1$ }

PUSH{ $R_2$ }

PUSH{ $R_3$ }

POP{ $R_1$ }

POP{ $R_2$ }

POP{ $R_3$ }

After execution, the content of registers  $R_1$ ,  $R_2$ ,  $R_3$  are

(a)  $R_1 = 40H$ ,  $R_2 = 30H$ ,  $R_3 = 25H$

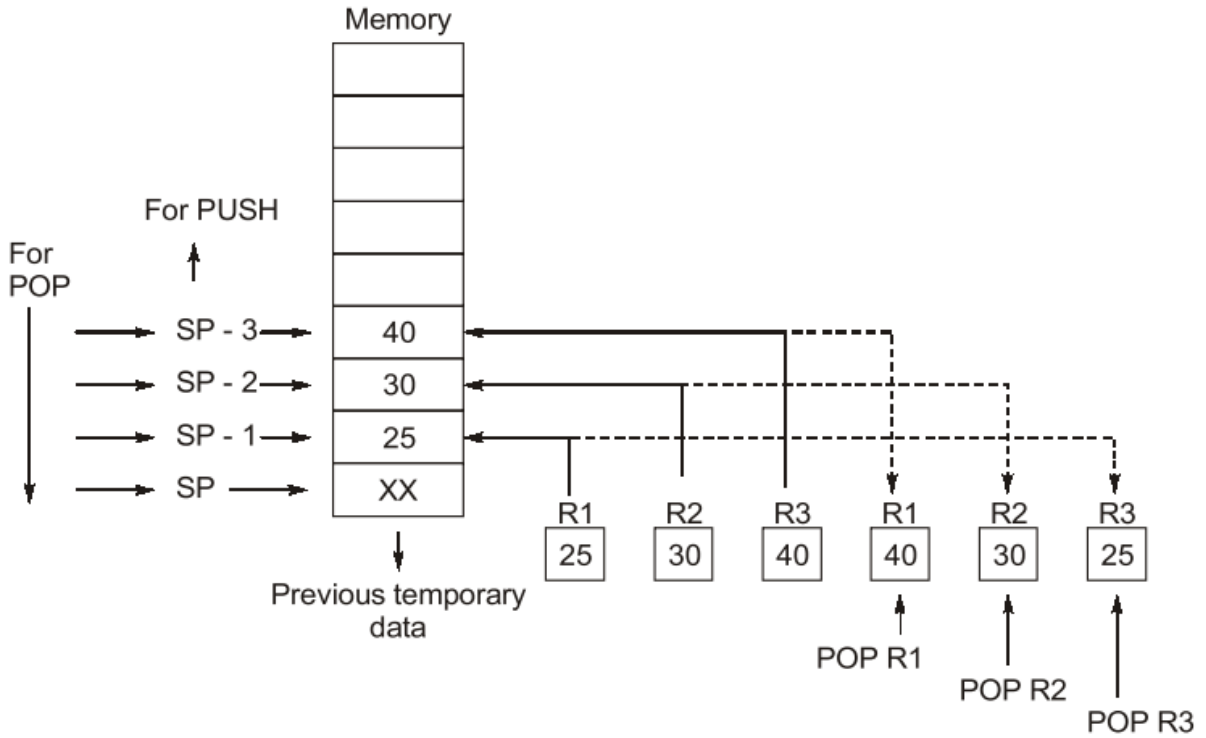
(b)  $R_1 = 25H$ ,  $R_2 = 30H$ ,  $R_3 = 40H$

(c)  $R_1 = 30H$ ,  $R_2 = 40H$ ,  $R_3 = 25H$

(d)  $R_1 = 40H$ ,  $R_2 = 25H$ ,  $R_3 = 30H$

Ans. a

Exp:



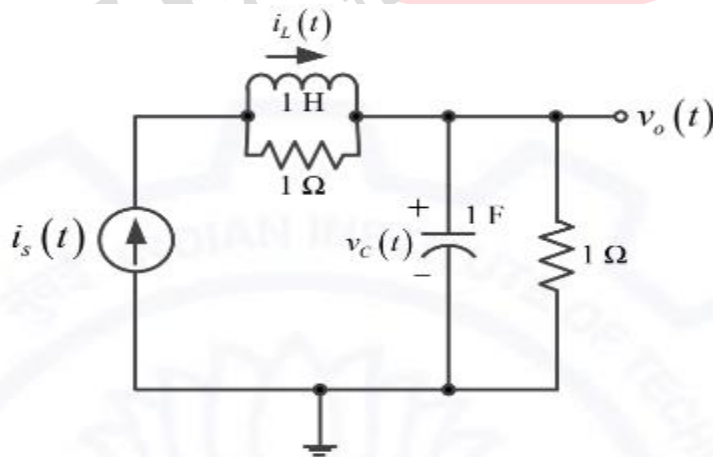
For PUSH SP is decremented and for POP SP is incremented.

$$\therefore [R_1] = 40$$

$$[R_2] = 30$$

$$[R_3] = 25$$

33. The electrical system shown in the figure converts input source current  $i_s(t)$  to output voltage  $v_o(t)$ .



Current  $i_L(t)$  in the inductor and voltage  $v_c(t)$  across the capacitor are taken as the state variables, both assumed to be initially equal to zero, i.e.,  $i_L(0)$  and  $v_c(0) = 0$ . The system is

(a) completely state controllable as well as completely observable

- (b) completely state controllable but not observable
- (c) completely observable but not state controllable
- (d) neither state controllable nor observable

Ans. d

Exp:

$$i_s = v_i + v_c$$

$$\therefore v_i = -v_c + i_s$$

$$v_L = Li_L$$

$$v_L = (i_s - i_L)$$

$$Li_L = i_s - i_L$$

$$i_L = -i_L + i_s$$

$$v_o = v_c$$

$$X = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} X + \begin{bmatrix} 1 \\ 2 \end{bmatrix} U$$

$$Y = [0 \quad 1]X + [0]U$$

$$A = -I$$

$$Q_c = [B \quad AB] = \begin{bmatrix} 1 & -1 \\ 1 & -1 \end{bmatrix} \Rightarrow |Q_c| = 0$$

$$Q_o = [C^T \quad A^T C^T] = \begin{bmatrix} 0 & 0 \\ 1 & -1 \end{bmatrix} \Rightarrow |Q_o| = 0$$

34. A digital transmission system uses a (7, 4) systematic linear Hamming code for transmitting data over a noisy channel. If three of the message-codeword pairs in this code ( $m_i ; c_i$ ), where  $c_i$  is the codeword corresponding to the  $i^{\text{th}}$  message  $m_i$ , are known to be (1 1 0 0 ; 0 1 0 1 1 0 0), (1 1 1 0 ; 0 0 1 1 1 1 0) and (0 1 1 0 ; 1 0 0 0 1 1 0), then which of the following is a valid codeword in this code?

- (a) 1 1 0 1 0 0 1
- (b) 1 0 1 1 0 1 0
- (c) 0 0 0 1 0 1 1
- (d) 0 1 1 0 1 0 0

Ans. c

Exp:

Given codewords:

$$\left. \begin{array}{l} C_1 = 0101100 \\ C_2 = 0011110 \\ C_3 = 1000110 \end{array} \right\}$$

In given above codewords, first  $n - k = 3$  bits are parity bits and last  $K = 4$  bits are message bits.

Given is (7, 4) systematic linear hamming code. For a linear code, sum of two codewords belong to the code is also a codeword belonging to the code.

$$C_1 \oplus C_2 = 0110010 = C_4$$

$$C_2 \oplus C_3 = 1011000 = C_5$$

$$C_1 \oplus C_3 = 1101010 = C_6$$

$$C_3 \oplus C_4 = 1110100 = C_7$$

Based on codewords  $C_6$  and  $C_7$  options (b) & (d) are incorrect.

$$\text{Given codewords in the form of} \quad \Rightarrow \quad \underbrace{P_1 \ P_2 \ P_3}_{\text{Paritybits}} \ \underbrace{d_1 \ d_2 \ d_3 \ d_4}_{\text{Messagebits}}$$

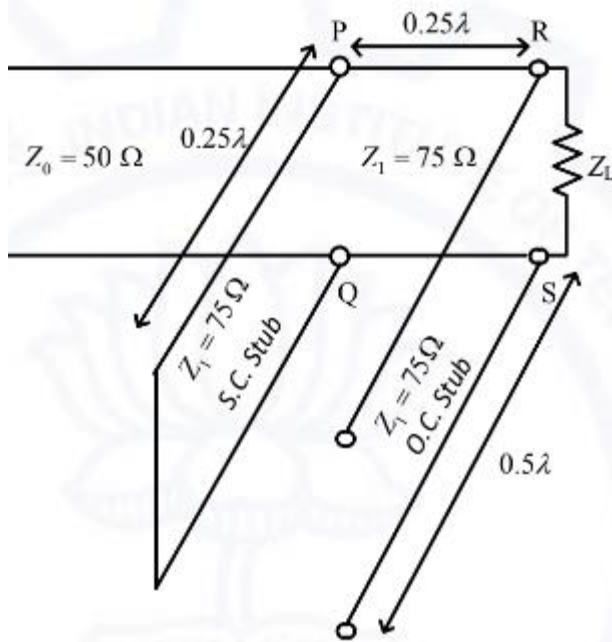
$$\text{From observation} \quad \Rightarrow \quad P_1 = d_1 \oplus d_2 \oplus d_4$$

$$P_2 = d_2 \oplus d_3 \oplus d_4$$

$$P_3 = d_1 \oplus d_2 \oplus d_3$$

From given options, only (c) satisfies the relation.

35. The impedance matching network shown in the figure is to match a lossless line having characteristic impedance  $Z_0 = 50 \ \Omega$  with a load impedance  $Z_L$ . A quarter-wave line having a characteristic impedance  $Z_1 = 75 \ \Omega$  is connected to  $Z_L$ . Two stubs having characteristic impedance of  $75 \ \Omega$  each are connected to this quarter-wave line. One is a short-circuited (S.C.) stub of length  $0.25\lambda$  connected across PQ and the other one is an open-circuited (O.C.) stub of length  $0.5\lambda$  connected across RS.



The impedance matching is achieved when the real part of  $Z_L$  is

- (a) 112.5  $\Omega$
- (b) 75.0  $\Omega$
- (c) 50.0  $\Omega$
- (d) 33.3  $\Omega$

Ans. a

Exp:

$$Z_{in \lambda/4} = \frac{Z_o^2}{Z_L} = \frac{(75)^2}{0} = \infty \quad \left[ \text{for } \frac{\lambda}{4} T_x \text{ line} \right]$$

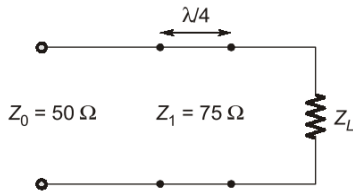
Given  $Z_L$  of  $\frac{\lambda}{4}$  line is 0(SC)

$$Z_{in \lambda/4} = Z_L = \infty \quad \left[ \text{for } \frac{\lambda}{2} T_x \text{ line} \right]$$

Given  $Z_L$  of  $\frac{\lambda}{2}$  line is  $\infty$  (OC)

The input impedance  $\frac{\lambda}{4}$  transmission line, as well as  $\frac{\lambda}{2}$  transmission line is  $\infty$ , and they are in parallel with main transmission line, so they are not effective for main Transmission line.

Final configuration of given line is



For impedance matching,  $Z_L = \frac{Z_1^2}{Z_0} = \frac{(75)^2}{50} = 112.5$

**Q.36 – Q.55 Numerical Answer Type (NAT), carry TWO mark each (no negative marks).**

36. A real  $2 \times 2$  non-singular matrix A with repeated eigenvalue is given as  $A = \begin{bmatrix} x & -3.0 \\ 3.0 & 4.0 \end{bmatrix}$  where  $x$  is a real positive number. The value of  $x$  (rounded off to one decimal place) is \_\_\_\_\_

Ans. 10.0

Exp:

Given matrix is

$$A = \begin{bmatrix} x & -3.0 \\ 3.0 & 4.0 \end{bmatrix}$$

Characteristic equation is

$$|A - \lambda I| = \begin{vmatrix} x - \lambda & -3 \\ 3 & 4 - \lambda \end{vmatrix} = 0$$

$$\lambda^2 - (4 + x)\lambda + (4x + 9) = 0$$

This is quadratic equation so it can be solved in the way given below:

$$b^2 - 4ac = 0$$

$$(4 + x^2) - 4(4x + 9) = 0$$

$$x^2 - 8x + 20 = 0$$

$$x = -2, 10$$

Take positive quantity,  $x = 10$

37. For a vector field  $D = \rho \cos^2 \phi \mathbf{a}_\rho + z^2 \sin^2 \phi \mathbf{a}_\phi$  in a cylindrical coordinate system  $(\rho, \phi, z)$  with unit vectors  $\mathbf{a}_\rho, \mathbf{a}_\phi$  and  $\mathbf{a}_z$ , the net flux of  $D$  leaving the closed surface of the cylinder ( $\rho = 3, 0 \leq z \leq 2$ ) (rounded off to two decimal places) is \_\_\_\_\_



Ans. 56.50 – 56.60

Exp:

**Method 1:**

Electric flux crossing the closed surface is

$$\psi = \iiint \vec{D} \cdot \vec{dS}$$

Electric flux crossing  $\rho = 3$  cylindrical surface is

$$\begin{aligned} \psi|_{\rho=3} &= \iiint (\rho \cos^2 \phi \hat{a}_\rho) \cdot (\rho d\phi dz) \hat{a}_\rho \\ &= 3^2 \int_{\phi=0}^{2\pi} \cos^2 \phi d\phi \int_{z=0}^2 dz \\ &= 9 \frac{1}{2} (2\pi)(2) = 56.55 \text{ Coulomb} \end{aligned}$$

**Method 2:**

$$D = \rho \cos^2 \phi a_\rho + z^2 \sin^2 \phi a_\phi$$

Electric flux crossing the closed surface is

$$\psi = \iiint \vec{D} \cdot \vec{dS} = \iiint (\vec{\nabla} \cdot \vec{D}) dv$$

$$\vec{\nabla} \cdot \vec{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z}$$

$$= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho \rho \cos^2 \phi) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (z^2 \sin^2 \phi) + 0$$

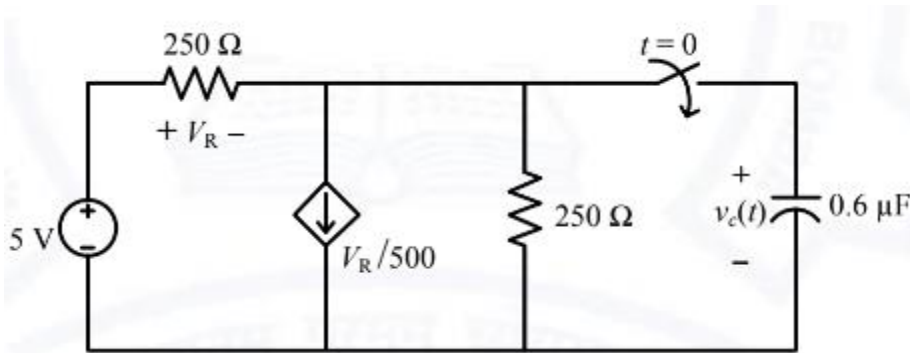
$$= \frac{1}{\rho} (2\rho) (\cos^2 \phi) + \frac{1}{\rho} (z^2 2 \sin \phi \cos \phi) = 2 \cos^2 \phi + \frac{z^2}{\rho} \sin 2\phi$$

$$\iiint (\vec{\nabla} \cdot \vec{D}) dv = \iiint 2 \cos^2 \phi (\rho d\rho d\phi dz) + \iiint \left( \frac{z^2}{\rho} \sin 2\phi \right) \rho d\rho d\phi dz$$

$$= 2 \int_{\rho=0}^3 \rho d\rho \int_{\phi=0}^{2\pi} \left( \frac{1 + \cos 2\phi}{2} \right) d\phi \int_{z=0}^2 dz + \int_{\rho=0}^2 d\rho \int_{\phi=0}^{2\pi} \sin 2\phi d\phi \int_{z=0}^2 z^2 dz$$

$$= 2 \left( \frac{\rho^2}{2} \right)_{\rho=0}^3 \frac{1}{2} (2\pi) (z)_{z=0}^2 + 0 = 2 \left( \frac{3^2}{2} \right) (2\pi) = 18\pi \text{ (Coulomb)} = 56.55 \text{ Coulomb}$$

38. In the circuit shown in the figure, the switch is closed at time  $t = 0$ , while the capacitor is initially charged to  $-5\text{ V}$  (i.e.,  $v_c(0) = -5\text{ V}$ ).



The time after which the voltage across the capacitor becomes zero (rounded off to three decimal places) is \_\_\_\_\_ ms.

Ans. 0.132 – 0.146

Exp:

$$V_c(0^-) = -5\text{V}, V_c(0^+) = -5\text{V}$$

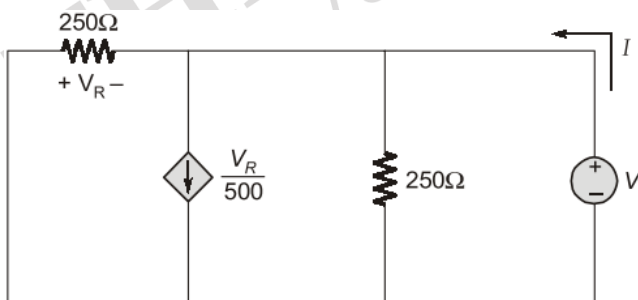
As  $t \rightarrow \infty$ , capacitor acts as an O. C.

KCL at node

$$\frac{V_c(\infty) - 5}{250} + \frac{V_R}{500} + \frac{V_c(\infty)}{250} = 0$$

$$V_c(\infty) = \frac{5}{3}\text{V}$$

Time constant ( $\tau$ ) =  $R_{eq} C$ .



$$I = \frac{V}{250} + \frac{V_R}{500} + \frac{V}{250}$$

$$V_R = -V$$

$$I = \frac{V}{250} - \frac{V}{500} + \frac{V}{250}$$

$$\frac{V}{I} = \frac{500}{3} \Omega \quad ; \quad R_{eq} = \frac{500}{3} \Omega$$

$$\tau = \frac{500}{3} \times 0.6 \mu = 0.1 \times 10^{-3}$$

$$v_c(t) = v_c(\infty) + (v_c(0) - v_c(\infty))e^{-t/\tau}$$

$$v_c(t) = \frac{5}{3} + \left(-5 - \frac{5}{3}\right)e^{-t/0.1 \times 10^{-3}}$$

$$0 = \frac{5}{3} - \frac{20}{3}e^{-10000t}$$

$$t = 0.1386 \text{ m sec}$$

39. The exponential Fourier series representation of a continuous-time periodic signal  $x(t)$  is defined as

$$x(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_0 t}$$

where  $\omega_0$  is the fundamental angular frequency of  $x(t)$  and the coefficients of the series are  $a_k$ . The following information is given about  $x(t)$  and  $a_k$ .

I.  $x(t)$  is real and even, having a fundamental period of 6

II. The average value of  $x(t)$  is 2

$$\text{III. } a_k = \begin{cases} k, & 1 \leq k \leq 3 \\ 0, & k > 3 \end{cases}$$

The average power of the signal  $x(t)$  (rounded off to one decimal place) is \_\_\_\_\_

Ans. 31.9 – 32.1

Exp:

1.  $x(t)$  is real and even so  $a_k$  is also real and even  $a_k = a_{-k}$

2. Average of  $x(t)$  is 2, i.e.,  $a_0 = 2$ .

$$\begin{array}{llll} 3. x(t) \rightarrow a_k = k & 1 \leq k \leq 3 & a_1 = 1 & a_{-1} = 1 \\ & 0 & k > 3 & a_2 = 2 & a_{-2} = 2 \\ & & & a_3 = 3 & a_{-3} = 3 \end{array}$$

4.  $T_0 = 6$

Parsval's Power Theorem

$$\frac{1}{T} \int_0^T |x(t)|^2 dt = \sum_{n=-\infty}^{\infty} |a_k|^2$$

$$P_{x(t)} = \sum_{n=-\infty}^{\infty} |a_k|^2 = |a_{-3}|^2 + |a_{-2}|^2 + |a_{-1}|^2 + |a_0|^2 + |a_1|^2 + |a_2|^2 + |a_3|^2$$

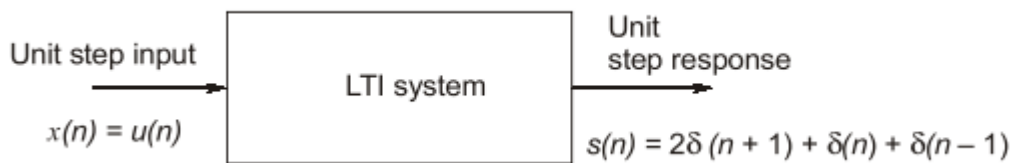
$$= |a_0|^2 + 2|a_1|^2 + 2|a_2|^2 + 2|a_3|^2$$

$$= 2 \times 1^2 + 2(2)^2 + 2(3)^2 + 2^2 = 32$$

40. For a unit step input  $u[n]$ , a discrete-time LTI system produces an output signal  $(2\delta[n + 1] + \delta[n] + \delta[n - 1])$ . Let  $y[n]$  be the output of the system for an input  $\left(\left(\frac{1}{2}\right)^n u[n]\right)$ . The value of  $y[0]$  is \_\_\_\_\_

Ans. 0

Exp:



The impulse response  $h(n) = s(n) - s(n - 1)$

$$h(n) = 2\delta(n + 1) + \delta(n) + \delta(n - 1) - 2\delta(n) - \delta(n - 1) - \delta(n - 1 - 1)$$

$$= 2\delta(n + 1) + \delta(n) + \delta(n - 1) - 2\delta(n) - \delta(n - 1) - \delta(n - 2)$$

$$= 2\delta(n + 1) - \delta(n) - \delta(n - 2)$$

For input  $x_1(n) = (1/2)^n u(n)$  then output  $y_1(n) = x_1(n) * h(n)$

$$y_1(n) = \left(\frac{1}{2}\right)^n u(n) * [2\delta(n + 1) - \delta(n) - \delta(n - 2)]$$

$$y_1(n) = \left(\frac{1}{2}\right)^n u(n) * 2\delta(n + 1) - \left(\frac{1}{2}\right)^n u(n) * \delta(n) - \left(\frac{1}{2}\right)^n u(n) * \delta(n - 2)$$

$$y_1(n) = 2\left(\frac{1}{2}\right)^{n+1} u(n + 1) - \left(\frac{1}{2}\right)^n u(n) - \left(\frac{1}{2}\right)^{n-2} u(n - 2)$$

$$y_1(n)|_{n=0} = 2\left(\frac{1}{2}\right)^1 u(1) - \left(\frac{1}{2}\right)^0 u(0) - \left(\frac{1}{2}\right)^{-2} u(-2)$$

$$y_1(n) = 0$$

41. Consider the signals  $x[n] = 2^{n-1} u[-n + 2]$  and  $y[n] = 2^{-n+2} u[n + 1]$ , where  $u[n]$  is the unit step sequence. Let  $X(e^{j\omega})$  and  $Y(e^{j\omega})$  be the discrete-time Fourier transform of  $x[n]$  and  $y[n]$ , respectively. The value of the integral

$$\frac{1}{2\pi} \int_0^{2\pi} X(e^{j\omega}) Y(e^{-j\omega}) d\omega$$

(rounded off to one decimal place) is \_\_\_\_\_

Ans. 7.9 – 8.1

Exp:

$$x[n] = 2^{n-1} u[-n + 2]$$

$$y[n] = 2^{-n+2} u[-n + 1]$$

$$y[-n] = 2^{n+2} u[-n + 1]$$

$$V = \frac{1}{2\pi} \int_0^{2\pi} X(e^{j\omega}) Y(e^{-j\omega}) d\omega \quad \text{(i)}$$

$$z[n] = x[n] * y[-n]$$

$$z[n] \rightarrow Z(e^{j\omega})$$

$$z[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} Z(e^{j\omega}) e^{j\omega n} d\omega$$

$$z[0] = \frac{1}{2\pi} \int_{-\pi}^{\pi} Z(e^{j\omega}) d\omega \quad (n=0) \quad \text{(ii)}$$

Compare equations (i) and (ii),

$$z[0] = V$$

$$Z(e^{j\omega}) = X(e^{j\omega}) Y(e^{-j\omega})$$

Apply IDTFT,  $z[n] = x[n] * y[-n] = x[n] * p[n]$

$$\therefore p[n] = y[-n] = 2^{n+2} u[-n + 1]$$

$$z[n] = \sum_{k=-\infty}^{\infty} 2^{k-1} u[-k+2] 2^{n-k+2} u[-n+k+1]$$

$$= \sum_{k=-\infty}^2 2^{k-1} 1 \cdot 2^{n-k+2} u[-n+k+1]$$

$$= \sum_{k=-\infty}^2 2^{k-1+n-k+2} u[-n+k+1]$$

$$z[n] = \sum_{k=-\infty}^2 2^{n+1} u[-n+k+1]$$

$$V = z[0] = \sum_{k=-\infty}^2 2^1 u[k+1] = 2 \sum_{k=-1}^2 1 = 2[1+1+1+1] = 8$$

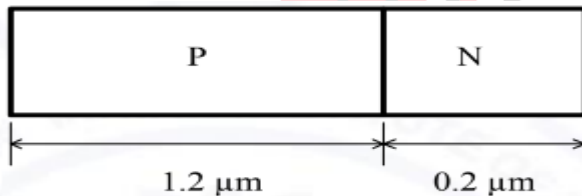
42. A silicon P-N junction is shown in the figure. The doping in the P region is  $5 \times 10^{16} \text{ cm}^{-3}$  and doping in the N region is  $10 \times 10^{16} \text{ cm}^{-3}$ . The parameters given are

Built-in voltage ( $\Phi_{bi}$ ) = 0.8 V

Electron charge (q) =  $1.6 \times 10^{-19} \text{ C}$

Vacuum permittivity ( $\epsilon_0$ ) =  $8.85 \times 10^{-12} \text{ F/m}$

Relative permittivity of silicon ( $\epsilon_{si}$ ) = 12



The magnitude of reverse bias voltage that would completely deplete one of the two regions (P or N) prior to the other (rounded off to one decimal place) is \_\_\_\_\_ V.

Ans. 8.1 – 8.4

Exp:

Given :  $N_A = 5 \times 10^{16} \text{ cm}^{-3}$  ;  $N_D = 10 \times 10^{16} \text{ cm}^{-3}$

Built-in potential,  $\phi_{bi} = 0.8 \text{ V}$

Electron charge,  $q = 1.6 \times 10^{-19} \text{ C}$

Vacuum permittivity,  $\epsilon_0 = 8.85 \times 10^{-12} \text{ F/m} = 8.85 \times 10^{-14} \text{ F/cm}$

Relative permittivity silicon,

$$\epsilon_{Si} = 12$$

Doping on both sides is comparable, so smaller region would deplete first.

So, depletion region width on N-side =  $x_n = 0.2 \mu\text{m}$

$$\Rightarrow x_n = 0.2 \times 10^{-4} \text{ cm}$$

$$x_n = \sqrt{\frac{2\epsilon_{Si}}{q} \left(\frac{N_A}{N_D}\right) \left(\frac{1}{N_A + N_D}\right) (\phi_{bi} + V_R)}$$

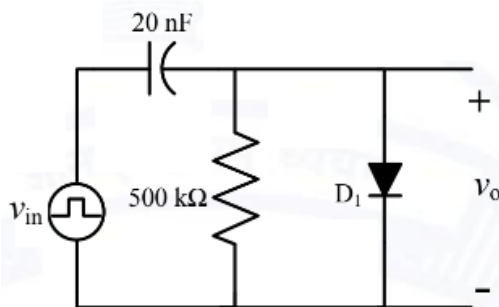
Where,  $V_R \rightarrow$  Magnitude of reverse bias potential.

$$\Rightarrow 0.2 \times 10^{-4} = \sqrt{\frac{2 \times 12 \times 8.85 \times 10^{-14}}{1.6 \times 10^{-19}} \times \frac{5 \times 10^{16}}{10 \times 10^{16}} \times \frac{1}{(15 \times 10^{16})} (\phi_{bi} + V_R)}$$

$$\Rightarrow \phi_{bi} + V_R = 9.039$$

$$V_R = 9.039 - 0.8 = 8.3 \text{ V}$$

43. An asymmetrical periodic pulse train  $v_{in}$  of 10 V amplitude with on-time  $T_{ON} = 1 \text{ ms}$  and off-time  $T_{OFF} = 1 \mu\text{s}$  is applied to the circuit shown in the figure. The diode  $D_1$  is ideal.

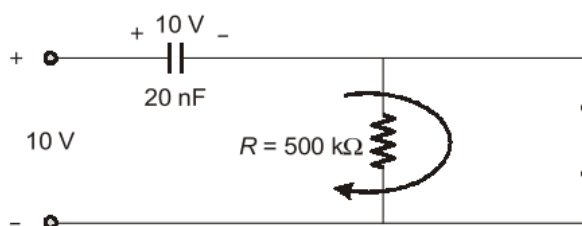


The difference between the maximum voltage and minimum voltage of the output waveform  $v_o$  (in integer) is \_\_\_\_\_ V.

Ans. 10

Exp:

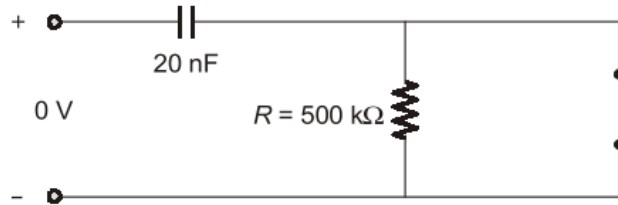
$V_{in} = 10 \text{ V}$  : Diode is ON



∴ Capacitor charges upto 10 V,

$$V_C = 10 \text{ V}$$

$V_{in} = 0$ ; Diode is OFF



Discharging time constant =  $R \times C = 10 \text{ m sec}$

$T_{\text{discharging}} \gg \tau_{\text{OFF}}$

Capacitor discharges negligibly

$$\therefore V_C = 10 \text{ V}$$

In steady state,  $V_C = 10 \text{ V}$

$$V_{\text{out}} = V_{in} - V_C = V_{in} - 10 \text{ V}$$

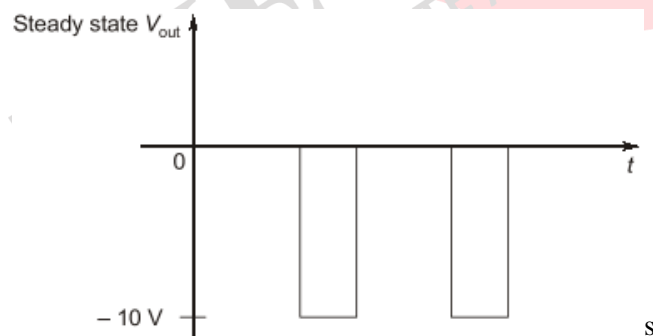
When  $V_{in} = 10 \text{ V}$

$$V_{\text{out}} = 0$$

$$V_{in} = 10 \text{ V}$$

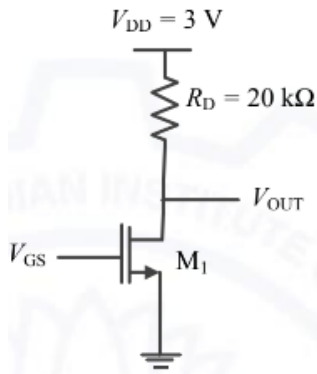
$$V_{\text{out}} = -10 \text{ V}$$

$$V_{\text{out(max)}} - V_{\text{out(min)}} = 10 \text{ V}$$



44. For the transistor  $M_1$  in the circuit shown in the figure,  $\mu_n C_{ox} = 100 \mu\text{A}/\text{V}^2$  and  $(W/L) = 10$ , where  $\mu_n$  is the mobility of electron,  $C_{ox}$  is the oxide capacitance per unit area,  $W$  is the width and  $L$  is the length.





The channel length modulation coefficient is ignored. If the gate-to-source voltage  $V_{GS}$  is 1 V to keep the transistor at the edge of saturation, then the threshold voltage of the transistor (rounded off to one decimal place) is \_\_\_\_\_ V.

Ans. 0.5

Exp:

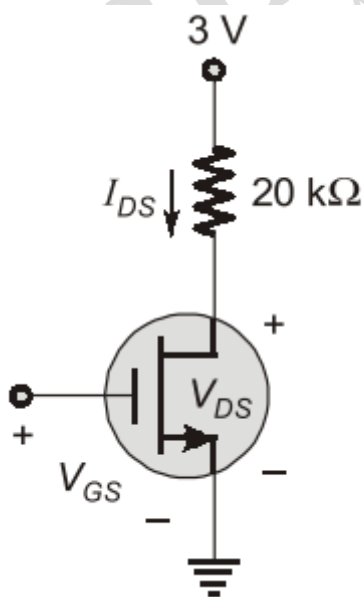
$$I_{DS} = \frac{\mu_n C_{ox}}{2} \times \frac{W}{L} (V_{GS} - V_T)^2$$

Given,  $V_{GS} = 1 \text{ V}$

$$I_{DS} = \frac{1}{2} (1 - V_T)^2$$

$$V_{DS} = 3 - 20 \times I_{DS}$$

$$V_{DS} = 3 - \frac{20}{2} (1 - V_T)^2 = 3 - 10(1 - V_T)^2$$



MOSFET operates in saturation if

$$V_{DS} \geq V_{GS} - V_T$$

So, we take,  $V_{DS} = V_{GS} - V_T$

$$V_{GS} - V_T = V_{DS} = 3 - 10(1 - V_T)^2$$

Let,  $1 - V_T = x$

$$3 - 10x^2 = x$$

$$x = 0.5 \text{ and } -0.6$$

For  $x = 0.5$

$$1 - V_T = 0.5$$

$$V_T = 0.5 \text{ V}$$

$$x = -0.6$$

$$V_T = 1.6 \text{ V}$$

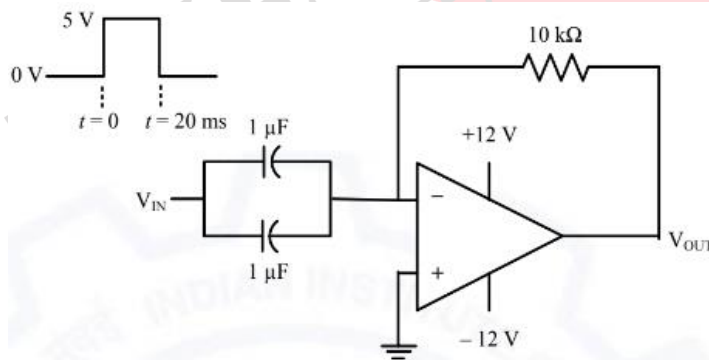
But  $V_{GS} > V_T$

or  $V_T < V_{GS}$

i.e.,  $V_T < 1$

$$\therefore V_T = 0.5 \text{ V}$$

45. A circuit with an ideal OPAMP is shown in the figure. A pulse  $V_{IN}$  of 20 ms duration is applied to the input. The capacitors are initially uncharged.



The output voltage  $V_{OUT}$  of this circuit at  $t = 0^+$  (in integer) is \_\_\_\_\_ V.

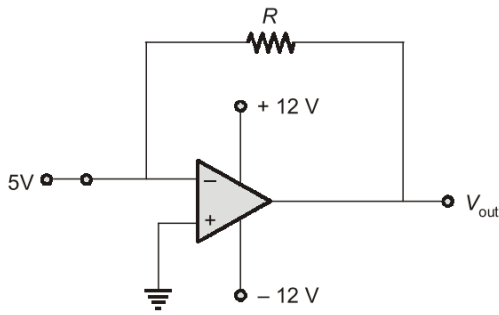
Ans. -12

Exp:

At,  $t = 0^+$  : Capacitor is short circuit

$$\therefore V^- = V_{in} = 5 \text{ V}$$

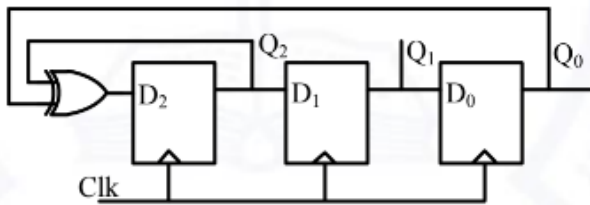
$V^+ = 0 \text{ V}$



If  $V^- > V^+$

$V_{out} = -V_{sat} = -12 \text{ V}$

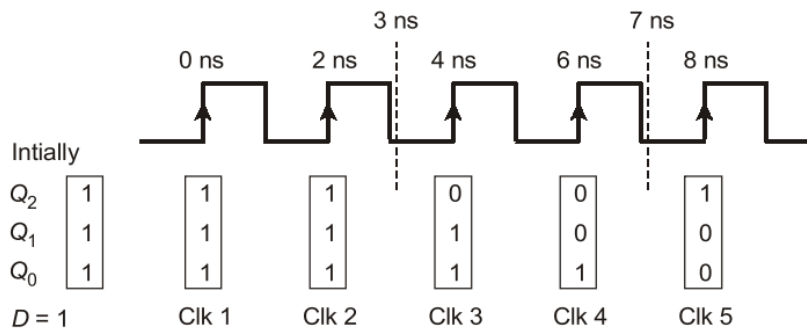
46. The propagation delay of the exclusive-OR (XOR) gate in the circuit in the figure is 3 ns. The propagation delay of all the flip-flops is assumed to be zero. The clock (Clk) frequency provided to the circuit is 500 MHz.



Starting from the initial value of the flip-flop outputs  $Q_2Q_1Q_0 = 1 1 1$  with  $D_2 = 1$ , the minimum number of triggering clock edges after which the flip-flop outputs  $Q_2Q_1Q_0$  becomes 1 0 0 (in integer) is \_\_\_\_\_

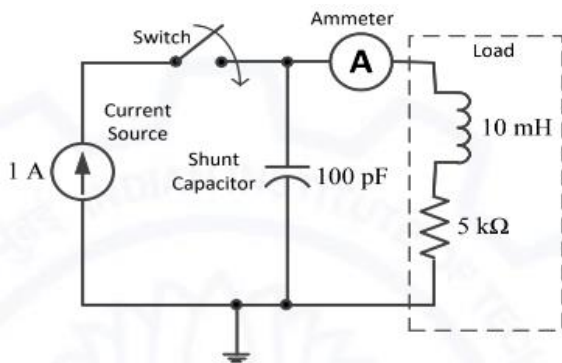
Ans. 5

Exp:



$\therefore$  Total clocks required = 5

47. The circuit in the figure contains a current source driving a load having an inductor and a resistor in series, with a shunt capacitor across the load. The ammeter is assumed to have zero resistance. The switch is closed at time  $t = 0$ .

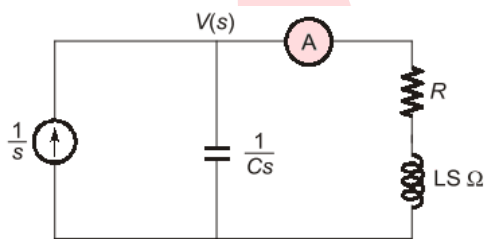


Initially, when the switch is open, the capacitor is discharged and the ammeter reads zero ampere. After the switch is closed, the ammeter reading keeps fluctuating for some time till it settles to a final steady value. The maximum ammeter reading that one will observe after the switch is closed (rounded off to two decimal places) is \_\_\_\_\_ A.

Ans. 1.40 – 1.50

Exp:

Apply Laplace transform,



$$\frac{1}{s} = \frac{V(s)}{1/Cs} + \frac{V(s)}{R + Ls} = V(s) \left[ Cs + \frac{1}{R + Ls} \right]$$

$$V(s) = \frac{(1/s)}{Cs + \frac{1}{R + Ls}} = \frac{(1/s)(R + Ls)}{LCs^2 + RCs + 1}$$

$$I(s) = \frac{(1/s)(R + Ls)}{LCs^2 + RCs + 1} \times \frac{1}{(R + Ls)} = \frac{1/LC}{s \left( s^2 + \frac{R}{L}s + \frac{1}{LC} \right)}$$

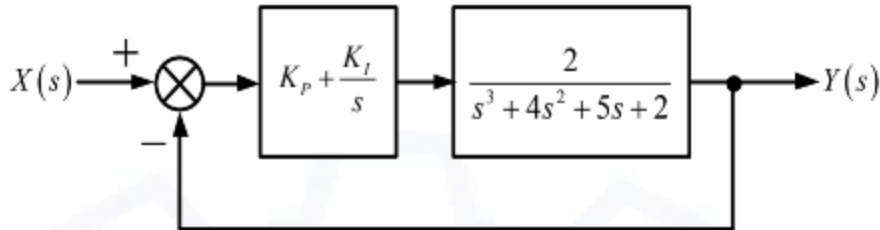
$$L = 10 \text{ mH}, C = 100 \text{ pF}, R = 5 \times 10^3 \Omega$$

$$\xi = \frac{R}{2} \sqrt{\frac{C}{L}} = \frac{5 \times 10^3}{2} \sqrt{\frac{100 \times 10^{-12}}{10 \times 10^{-3}}} = 0.25$$

$$\text{Max. Overshoot} = e^{-\pi\zeta/\sqrt{1-\zeta^2}} = 0.44$$

$$\text{Maximum value} = \text{Steady state} + \text{Max. Overshoot} = 1 + 0.44 = 1.44 \text{ A}$$

48. A unity feedback system that uses proportional-integral (PI) control is shown in the figure.



The stability of the overall system is controlled by tuning the PI control parameters  $K_p$  and  $K_I$ . The maximum value of  $K_I$  that can be chosen so as to keep the overall system stable or, in the worst case, marginally stable (rounded off to three decimal places) is \_\_\_\_\_

Ans. 3.125

Exp:

$$GH = \left( \frac{sK_p + K_I}{s} \right) \left( \frac{2}{s^3 + 4s^2 + 5s + 2} \right)$$

$$q(s) = s^4 + 4s^3 + 5s^2 + s(2 + 2K_p) + 2K_I$$

Necessary condition:  $K_p > -1$  ;  $K_I > 0$

$s^4$	1	5	$2K_I$
$s^3$	4	$2 + 2K_p$	
$s^2$	$\frac{18 - 2K_p}{4}$	$2K_I$	
$s^1$	$(9 - K_p)(1 + K_p) - 8K_I$		
$s^0$	$2K_I$		

Sufficient condition:

$$\frac{18 - 2K_p}{4} > 0$$

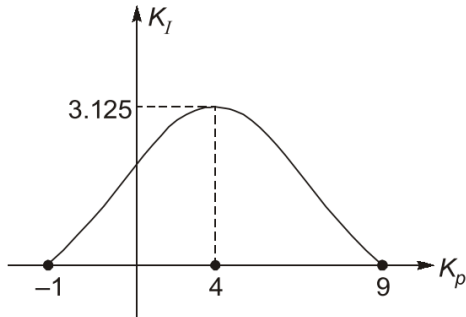
$$\Rightarrow K_p < 9$$

$$\therefore -1 < K_p < 9$$

$$(18 - 2K_p)(2 + 2K_p) - 32K_I > 0$$

$$32K_I < 36 + 32 K_p - 4 K_p^2$$

$$\therefore 0 < K_I < \frac{36 + 32 K_p - 4 K_p^2}{32}$$



$$\text{If } K_p = -1 \Rightarrow K_I = 0$$

$$\text{If } K_p = 9 \Rightarrow K_I = 0$$

$$\therefore \frac{dK_I}{dK_p} = 0$$

$$32 - 8K_p = 0 \Rightarrow K_p = 4$$

$\therefore$  For  $K_p = 4$ ,  $K_I$  is maximum, which is

$$K_I = \frac{36 + 32 \times 4 - 64}{32} = 3.125$$

For  $K_p = 4$ ,  $K_I < 3.125$  for stability

$$\therefore K_{I \max} = 3.125$$

49. A sinusoidal message signal having root mean square value of 4 V and frequency of 1 kHz is fed to a phase modulator with phase deviation constant 2 rad/volt. If the carrier signal is  $c(t) = 2 \cos(2\pi \times 10^6 t)$ , the maximum instantaneous frequency of the phase modulated signal (rounded off to one decimal place) is \_\_\_\_\_ Hz.

Ans. 1011313.5 – 1011313.9

Exp:

Given sinusoidal message signal  $\rightarrow V_{rms} = 4 \text{ V}$

$f_m = 1 \text{ kHz}$

$$V_{\text{peak}} = \sqrt{2} \times V_{rms} = \sqrt{2} \times 4 \text{ V}$$

$$m(t) = 4\sqrt{2} \sin 2\pi \times 10^3 t$$

$$K_p = 2 \text{ rad/volt}$$

$$c(t) = 2 \cos 2\pi \times 10^6 t$$

$$(f_i)_{\max} = f_c + \frac{K_p}{2\pi} \left[ \frac{d}{dt} m(t) \right]_{\max}$$

$$\frac{d}{dt} m(t) = 4\sqrt{2} \times (2\pi \times 10^3) \cos 2\pi \times 10^3 t$$

$$\left[ \frac{d}{dt} m(t) \right]_{\max} = 4\sqrt{2} \times 2\pi \times 10^3$$

$$(f_i)_{\max} = 10^6 + \frac{2}{2\pi} (4\sqrt{2} \times 2\pi \times 10^3) = 1011313.7 \text{ Hz}$$

50. Consider a superheterodyne receiver tuned to 600 kHz. If the local oscillator feeds a 1000 kHz signal to the mixer, the image frequency (in integer) is \_\_\_\_\_ kHz.

Ans. 1400

Exp:

$$f_s = 600 \text{ kHz}, f_l = 1000 \text{ kHz}, f_{si} = ?$$

$$\text{We have } f_l > f_s$$

$$\text{IF} = f_l - f_s = 400 \text{ kHz}$$

$$f_{si} = f_s + 2\text{IF} = 600 \text{ K} + 800 \text{ K} = 1400 \text{ kHz}$$

51. In a high school having equal number of boy students and girl students, 75% of the students study Science and the remaining 25% students study Commerce. Commerce students are two times more likely to be a boy than are Science students. The amount of information gained in knowing that a randomly selected girl student studies Commerce (rounded off to three decimal places) is \_\_\_\_\_ bits.

Ans. 3.320 – 3.325

Exp:

$$\text{Given, } P(S) = \frac{1}{2} \quad \text{and} \quad P(B) = \frac{1}{2}$$

$$P(C) = \frac{1}{4} \quad \text{and} \quad P(S) = \frac{3}{4}$$

Let probability of selected science student is a boy is  $P(B/S) = x$

Given that Commerce students are two time more likely to be a boy than are Science students.

Then, probability of selected Commerce student is a boy.

$$P\left(\frac{B}{C}\right) = 2x$$

We have to find probability of randomly selected girl studies Commerce, i.e.,

$$P\left(\frac{C}{G}\right) = \frac{P(C \cap G)}{P(G)} = \frac{P(C)P(G/C)}{P(G)}$$

$$P\left(\frac{C}{G}\right) = \frac{\frac{1}{4} \times P\left(\frac{G}{C}\right)}{\frac{1}{2}} \quad (i)$$

To find P(G/C), first we have to find P(B/C).

The probability of selected student is a boy

$$P(B) = P(S) P(B/S) + P(C) \times P(B/C)$$

$$\frac{1}{2} = \frac{3}{4} \times x + \frac{1}{4} \times 2x$$

$$x = \frac{2}{5}$$

$$\text{Then, } P(B/C) = 2x = \frac{4}{5}$$

We know that,

$$P\left(\frac{B}{C}\right) + P\left(\frac{G}{C}\right) = 1$$

$$P\left(\frac{G}{C}\right) = 1 - \frac{4}{5} = \frac{1}{5}$$

From eqn. (i)

$$P\left(\frac{C}{G}\right) = \frac{1}{4} \times \frac{1}{5} = \frac{1}{20}$$

The amount of information gained in knowing that a randomly selected girl studies Commerce



$$I\left(\frac{C}{G}\right) = \log_2 \frac{1}{P\left(\frac{C}{G}\right)}$$

$$= \log_2 10 = 3.322$$

52. A message signal having peak-to-peak value of 2 V, root mean square value of 0.1 V and bandwidth of 5 kHz is sampled and fed to a pulse code modulation (PCM) system that uses a uniform quantizer. The PCM output is transmitted over a channel that can support a maximum transmission rate of 50 kbps. Assuming that the quantization error is uniformly distributed, the maximum signal to quantization noise ratio that can be obtained by the PCM system (rounded off to two decimal places) is \_\_\_\_\_

Ans. 30.70 – 30.74

Exp:

$$V_{p-p} = 2V$$

$$\text{Root MSQ}[m(t)] = 0.1 \text{ V} \quad ; \quad f_m = 5 \text{ kHz}$$

$$\text{Channel capacity, } C = 50 \text{ kbps}$$

$$\text{Max } \frac{S}{N_Q} = ?$$

$$\text{Signal power, } S = \text{MSQ}[m(t)] = (0.1)^2 = 0.01$$

$$C \geq R_b \quad \Rightarrow \quad 50 \text{ kbps} \geq n f_s$$

$$\therefore f_s = nR = 2nf_m = 10 \text{ kHz}$$

$$n \leq 5 \quad \Rightarrow \quad n_{\max} = 5$$

$$N_Q = \frac{\Delta^2}{12}$$

$$\therefore \Delta = \frac{V_{p-p}}{2^n}$$

$$\Delta_{\min} = \frac{V_{p-p}}{2^{n_{\max}}} = \frac{2V}{2^5} = \frac{1}{16}$$

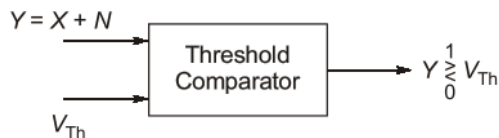
$$(N_Q)_{\min} = \frac{\Delta_{\min}^2}{12} = 3.25 \times 10^{-4}$$

$$\left(\frac{S}{N_Q}\right)_{\max} = \frac{S}{(N_Q)_{\min}} = \frac{0.01}{3.25 \times 10^{-4}} = 30.72$$

53. Consider a polar non-return to zero (NRZ) waveform, using +2 V and -2 V for representing binary '1' and '0' respectively, is transmitted in the presence of additive zero-mean white Gaussian noise with variance  $0.4 \text{ V}^2$ . If the a priori probability of transmission of a binary '1' is 0.4, the optimum threshold voltage for a maximum a posteriori (MAP) receiver (rounded off to two decimal places) is \_\_\_\_\_ V.

Ans. 0.03 – 0.05

Exp:



$$H_1 : X = +2V$$

$$H_0 : X = -2V$$

$$\text{Var}[N] = \sigma_n^2 = 0.4 \text{ V}^2$$

$$E[N] = 0$$

$$P(1) = 0.4$$

$$P(0) = 0.6$$

Opt  $V_{TH}$  by using MAP theorem

$$\frac{V_{Th} [a_1 - a_2]}{\sigma^2} - \frac{a_1^2 - a_2^2}{2\sigma^2} = \ln \frac{P(0)}{P(1)}$$

$$H_1 : a_1 = E[2 + N] = E[2] + E[N] = 2$$

$$H_0 : a_2 = E[-2 + N] = E[-2] + E[N] = -2$$

$$\sigma^2 = \text{Var}[Y] = \text{Var}[X + N] = \text{Var}[X] + \text{Var}[N] = 0 + 0.4 = 0.4$$

$$\frac{V_{Th} [2 + 2]}{0.4} - \frac{4 - 4}{2 \times 0.4} = \ln \frac{0.6}{0.4}$$

$$V_{Th} = 0.04 \text{ V}$$

54. A standard air-filled rectangular waveguide with dimensions  $a = 8 \text{ cm}$ ,  $b = 4 \text{ cm}$ , operates at  $3.4 \text{ GHz}$ . For the dominant mode of wave propagation, the phase velocity of the signal is  $v_p$ . The value (rounded off to two decimal places) of  $v_p/c$ , where  $c$  denotes the velocity of light, is \_\_\_\_\_.

Ans. 1.15 – 1.25

Exp:

$$f_{c10} = \frac{c}{2a} = \frac{3 \times 10^8}{2(8 \times 10^{-2})} = 1.875 \text{ GHz}$$

Guide phase velocity,  $V_p = \frac{c}{\sqrt{1 - \left(\frac{f_{c10}}{f}\right)^2}}$

$$\frac{V_p}{c} = \frac{1}{\sqrt{1 - \left(\frac{f_{c10}}{f}\right)^2}} = \frac{1}{\sqrt{1 - \left(\frac{1.875}{3.4}\right)^2}} = 1.20$$

55. An antenna with a directive gain of 6 dB is radiating a total power of 16 kW. The amplitude of the electric field in free space at a distance of 8 km from the antenna in the direction of 6 dB gain (rounded off to three decimal places) is \_\_\_\_\_ V/m.

Ans. 0.224 – 0.264

Exp:

$$G_d(\text{dB}) = 10 \log_{10}(G_d)$$

$$6 = 10 \log_{10} G_d$$

$$G_d = 3.981$$

$$E_m = \frac{\sqrt{60 G_d P_{rad}}}{r} = \sqrt{\frac{60(16 \times 10^3)(3.981)}{8 \times 10^3}} = 0.244 \text{ (V/m)}$$